

HINTS & SOLUTIONS

EXERCISE - 1

Single Choice

4. Molar conc. = $\frac{\text{no. of moles of O}_2}{\text{volume (in litre)}} = \frac{96}{32} \times \frac{1}{2} = 1.5 \text{ M}$

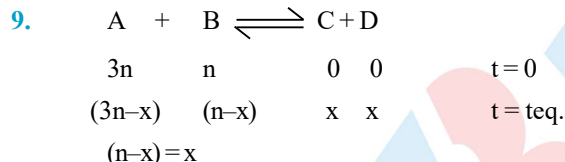
5. At equilibrium rates of backward and forward reactions become equal.

6. $K_c = \frac{\left[\frac{C}{V}\right]^2}{\left[\frac{B}{V}\right]\left[\frac{A}{V}\right]^3} \Rightarrow 9 = \frac{\left[\frac{2}{V}\right]^2}{\left[\frac{2}{V}\right]\left[\frac{2}{V}\right]^3} \Rightarrow V = 6 \text{ L}$

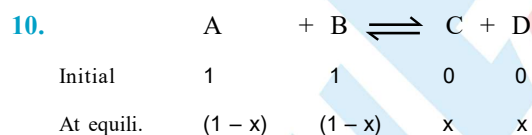
8. $A \xrightleftharpoons[K_2]{K_1} B \quad K_c = \frac{K_1}{K_2} = \frac{b+x}{a-x}$

$a-x \quad b+x \quad x = \frac{K_1 a - K_2 b}{K_1 + K_2}$

Therefore, (A) option is correct.



$n = 2x \quad x = \frac{n}{2}$

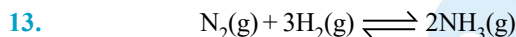


$\therefore K_c = \frac{[C][D]}{[A][B]} = 9$

$\therefore \frac{x \cdot x}{(1-x)^2} = 9 \text{ or } x^2 = 9 + 9x^2 - 18x \text{ or } 8x^2 - 18x + 9 = 0$

$\therefore x = \frac{3}{2} \text{ or } \frac{3}{4}$

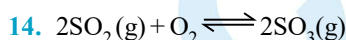
Hence, among the given options, the option (3) i.e., 0.75 is correct.



At equilibrium $\frac{P}{3} \quad P, \quad \frac{P}{3} + P + P_{NH_3} = 2P$

$P_{NH_3} = \frac{2P}{3} \quad K_p = \frac{\frac{2P}{3} \times \frac{2P}{3}}{\frac{P}{3} \times P^3} = \frac{1}{P^2} \cdot \frac{4}{3}$

$\Rightarrow K_p = \frac{4}{3P^2}$

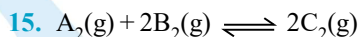


$K_p = 4.0 \text{ atm}^{-2}$

$K_p = \frac{(SO_3)^3}{(SO_2)^2(O_2)}$

Given that at equilibrium the amount of SO_2 and SO_3 is the same so

$\frac{(SO_3)^2}{(SO_2)^2(O_2)} = 4 \Rightarrow [O_2] = \frac{1}{4} = 0.25 \text{ atm.}$

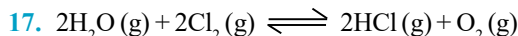


$P_{A_2} = 0.80 \text{ atm.}, \quad P_{B_2} = 0.4 \text{ atm.}$

Total pressure of the system = 2.8 atm.

$\therefore P_{C_2} = 2.8 - 0.8 - 0.4 = 1.6$

$K_p = \frac{P_{C_2}^2}{P_{A_2} \times P_{B_2}^2} = \frac{(1.6)^2}{0.8 \times (0.4)^2} = 20$



$K_p = 0.03 \text{ T} = 427^\circ\text{C} = 700 \text{ K}$

$K_p = K_c(RT)^1$

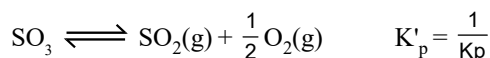
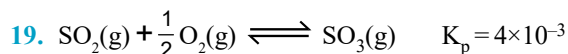
$K_c = \frac{K_p}{RT} = \left[\frac{0.03}{0.082 \times 700} \right]$

$K_c = 5.23 \times 10^{-4}$

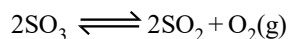


so, $\log \frac{K_p}{K_c} = \Delta n_g \log RT$

so, $\Delta n_g = -1.$

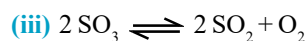
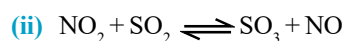
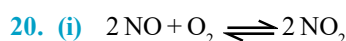


$$K'_p = \left(\frac{1}{4 \times 10^{-3}} \right)$$



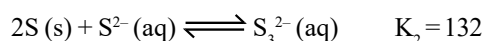
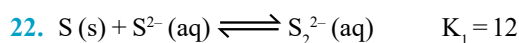
$$K''_p = (K'_p)^2 = \left[\frac{1}{4 \times 10^{-3}} \right]^2 = \left[\frac{1000}{4} \right]^2 = 6250 = 625 \times 10^2$$

6.25 × 10⁴ atm.

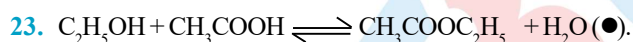


Now, $-2 \text{ (iii)} = \text{(i)} + \text{(ii)}$

so, $K_{C_3} \times K_{C_1} = 1/K_{C_2}$



Now, $\text{S}_2^{2-}(\text{aq}) + \text{S}(\text{s}) \rightleftharpoons \text{S}_3^{2-}(\text{aq}) \quad K_{\text{eq}} = \frac{K_2}{K_1} = \frac{132}{12} = 11$



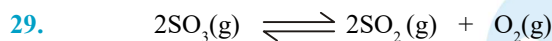
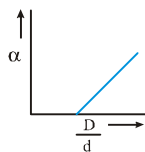
$$K_c = \frac{(0.33a) \times (0.33a)}{(0.67a) \times (0.67a)} = K_c = 1/4.$$

26. $\alpha = \left[\frac{D-d}{d} \right] ; \alpha = \left[\frac{D}{d} - 1 \right] ; \left(\frac{D}{d} \right) = \alpha + 1.$

$$\alpha = \frac{D-d}{(n-1)d} ; \alpha = \frac{D-d}{d} ; \alpha = \left(\frac{D}{d} \right) - 1.$$

The point at which $\alpha = 0$.

$$\left[\frac{D}{d} - 1 \right] = 0 ; \text{So, } \left(\frac{D}{d} \right) = 1.$$



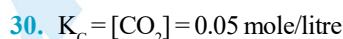
Total mole at eq. = $a \left(1 + \frac{\alpha}{2} \right)$

$$P_{\text{SO}_3} = \left(\frac{1-\alpha}{1+(\alpha/2)} \right) P_0 = \left[\frac{2(1-\alpha)}{2+\alpha} \right] \times P_0 ;$$

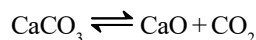
$$P_{\text{SO}_2} = \left(\frac{\alpha}{1+(\alpha/2)} \right) P_0 = \left(\frac{2\alpha}{2+\alpha} \right) \times P_0$$

$$P_{\text{O}_2} = \left(\frac{\alpha/2}{1+(\alpha/2)} \right) P_0$$

$$K_p = \frac{\frac{4\alpha^2(P_0)^2}{(2+\alpha)^2} \times \left(\frac{\alpha}{2+\alpha} \right) \times P_0}{\frac{4(1-\alpha)^2}{[2+\alpha]^2} \times (P_0)^2} = \left[\frac{\alpha^3 P_0}{(2+\alpha)(1-\alpha)^2} \right]$$



so moles of $\text{CO}_2 = 6.50 \times 0.05 \text{ moles} = 0.3250 \text{ moles}$



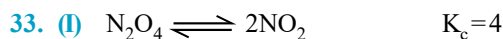
1 mole of $\text{CO}_2 = 1 \text{ mole of CaCO}_3$

$0.3250 \text{ moles of CO}_2 = 0.3250 \text{ moles of CaCO}_3$
 $= 0.3250 \times 100 \text{ gm of CaCO}_3 = 32.5 \text{ gm of CaCO}_3$



$P = P/2 \quad P = \frac{3P}{2} = 12$

so, $K_p = \frac{P^2}{(P/2)} = 2P = 2 \times 8 = 16 \text{ atm.}$



at point — A

$$Q = \frac{[\text{Product}]}{[\text{Reactant}]} = 0$$

So, Q have minimum value at point A.

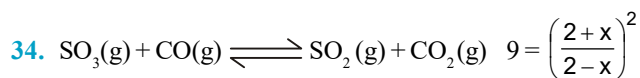
(III) at point $[N_2O_4] = [NO_2] = 0.1 \text{ M}$

$$Q = \frac{[NO_2]^2}{[N_2O_4]} = \frac{0.1 \times 0.1}{0.1} = 0.1$$

$$Q < K_c$$

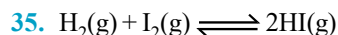
So, reaction proceeds left to right

(III) $K_c = Q$ at point [D & F].



$$\begin{array}{ccccccc} 2 & 2 & 2 & 2 & & & \\ 2+x & 2+x & 2-x & 2-x & x=1 & & \\ n_{eq} = 3+3+1+1 = 8 & & n(SO_3) + n(CO_2) = 4 & & & & \\ & & \frac{n(SO_2)}{n(CO)} = \frac{1}{2} < 1 & & & & \end{array}$$

Therefore, (D) option is correct.



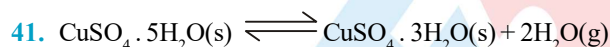
$$\log \frac{K_2}{K_1} = \frac{\Delta H}{2.303R} \left[\frac{1}{T_1} - \frac{1}{T_2} \right] ;$$

$$\log \frac{50}{66.9} = \frac{\Delta H}{2.303R} \left[\frac{1}{623} - \frac{1}{721} \right]$$

After calculation negative value of ΔH is obtained.

37. $\log K_2 / \log K_1 = \frac{-\Delta H}{2.303} \left[\frac{1}{T_2} - \frac{1}{T_1} \right]$

$\Delta H = \text{Positive}$.



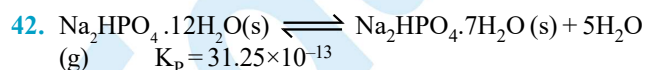
$$K_p = 2.25 \times 10^{-4}$$

$$K_p = p_{H_2O}^2 = 2.25 \times 10^{-4}$$

$$p_{H_2O} = 1.5 \times 10^{-2}$$

$$\text{Vapour pressure} = \frac{22.8}{760} = 3 \times 10^{-2} \quad \text{R.H.} = \frac{p_{H_2O}}{V.P.} \times 100 = 50\%$$

Therefore, (B) option is correct.



$$K_p = (P_{H_2O})^5$$

$$(P_{H_2O})^5 = 31.25 \times 10^{-13}$$

$$(P_{H_2O}) = (3125)^{1/5} \times (10^{-13})^{1/5}$$

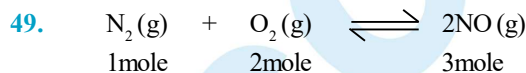
$$(P_{H_2O}) = 5 \times 10^{-3}$$

44. High temperature will favour backward reaction as reaction is exothermic. While on increasing pressure reaction will shift in direction higher density.

45. For constant volume, reaction quotient (Q) will remain constant.

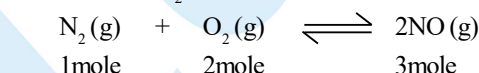
For constant pressure, reaction quotient (Q) will remain constant when $\Delta n_g = 0$.

47. On adding inert gas at constant pressure effect on equilibrium will be similar to as if volume of container has been increased.



$$K_c = \frac{(3)^2}{1 \times 2} = \left(\frac{9}{2}\right)$$

Let a mole of O_2 is added, Then,



$$t=0 \quad 1 \quad (2+a) \quad 3$$

$$[NO] = \left[\frac{3+2x}{100} \right] = 0.04 \quad ; \quad (3+2x) = 4.$$

$$2x = 1, \quad x = 0.5.$$

$$K_c = \frac{(3+2x)^2}{(1-x)(2+a-x)} = \frac{9}{2}.$$

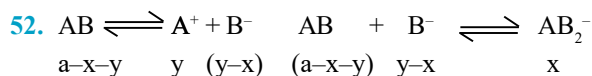
$$K_c = \frac{(4)^2}{0.5[(1.5)-a]} = \frac{9}{2}.$$

$$= \frac{16}{0.5(1.5+a)} = \frac{9}{2}.$$

$$= \frac{35}{4.5} = [1.5+a]$$

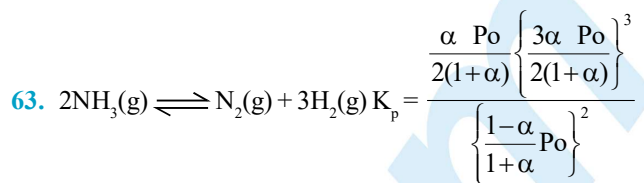
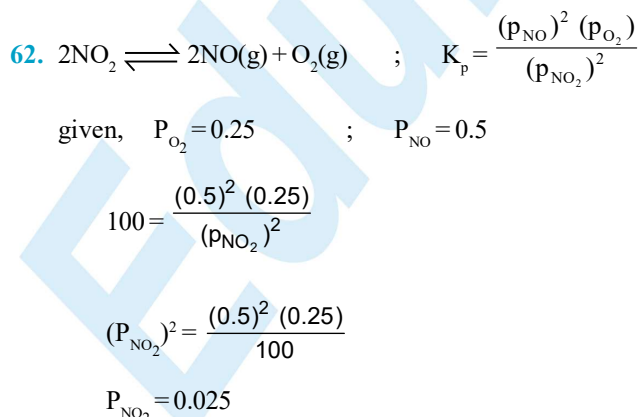
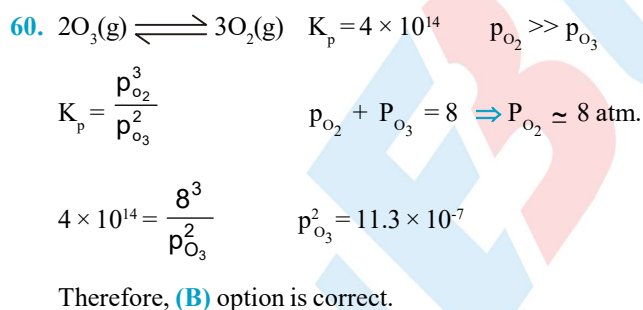
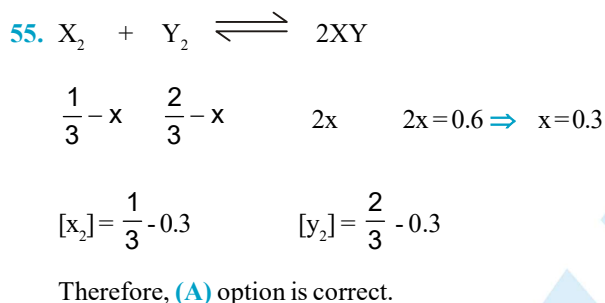
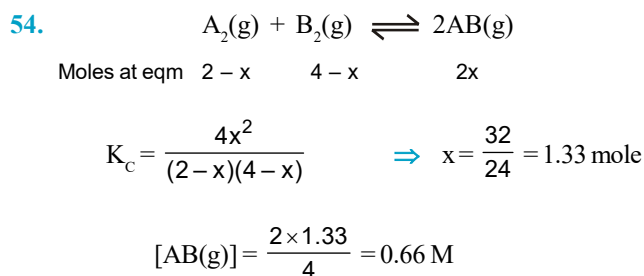
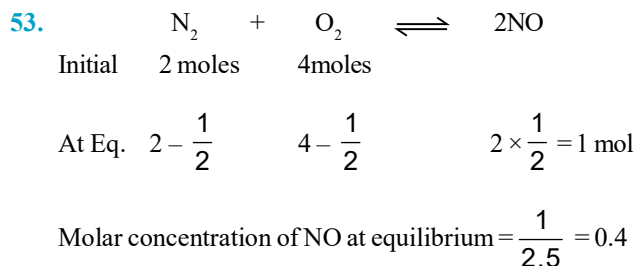
$$7.11 = 1.5 + a.$$

$$a = \frac{101}{18} = 5.61$$



$$K_1 = \frac{y(y-x)}{(a-x-y)} \quad K_2 = \frac{x}{(a-x-y)(y-x)}$$

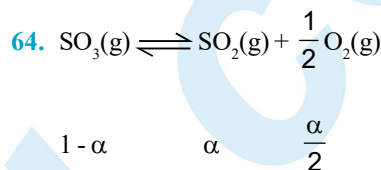
$$\frac{K_1}{K_2} = \frac{\left[\frac{y(y-x)}{(a-x-y)} \right]}{\frac{x}{(a-x-y)(y-x)}} \Rightarrow \frac{K_1}{K_2} = \frac{y}{x} (y-x)^2$$



$1 - \alpha$	$\frac{\alpha}{2}$	$\frac{3\alpha}{2}$
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$$1 - \alpha \approx 1 \text{ and } 1 + \alpha \approx 1 \Rightarrow 27 \times 10^{-8} p_0^2 = \frac{27}{16} p_0^2 \times \alpha^4$$

$$\alpha = 2 \times 10^{-2}$$

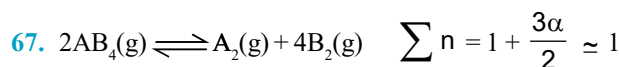


$$M_{\text{mix}} = \frac{0.9 \times 0.082 \times 1000}{1.23} = 60$$

$$M_{\text{mix}} = \frac{\alpha M_{\text{SO}_2} + \frac{\alpha}{2} M_{\text{O}_2} + (1 - \alpha) M_{\text{SO}_3}}{1 + \frac{\alpha}{2}}$$

$$1 + \frac{\alpha}{2} = \frac{80}{60} \quad \frac{\alpha}{2} = \frac{20}{60}$$

$$\alpha = \frac{2}{3}$$



$1 - \alpha$	$\frac{\alpha}{2}$	$2x$	$1 - \alpha \approx 1$
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$$K_p = \frac{\left(\frac{\alpha}{2} P \right) \left(\frac{2\alpha}{1} \times P \right)^4}{(P)^2} = 8P^3 \alpha^5$$



$$\text{Reaction Quotient, } Q_p = \frac{P_{\text{NH}_3}^2}{P_{\text{N}_2} (P_{\text{H}_2})^3} = \frac{3^2}{1 \times (2)^3} = \frac{9}{8}$$

$Q_p > K_p$, \therefore Reaction will go Backward.

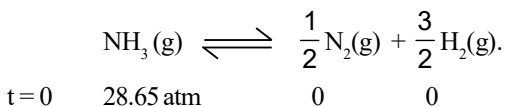
72. $P_1 = 15 \text{ atm}$; $T_1 = 300 \text{ K}$.

Equilibrium temperature is 300°C that is 573 K .

So first of all we have to calculate pressure of NH_3 at 573 K .

$$\frac{P_1}{T_1} = \frac{P_2}{T_2} = \frac{15}{300} = \frac{P_2}{573}$$

$P_2 = 28.65 \text{ atm}$ at 300°C .



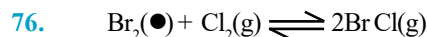
$$t = t_{\text{eq.}} \quad [28.65 - x] \text{ atm} \quad \frac{3}{2} x$$

But according to question.

$$P_{\text{total}} = 28.65 - x + \frac{x}{2} + \frac{3}{2} x \quad \text{or} \quad 28.65 + x = 40.11.$$

$$x = 11.46.$$

Degree of dissociation of $\text{NH}_3 = \frac{11.46}{28.65} = 0.4$.



$t = 0$	1	0
	$(1 - x)$	$2x$

$$K_p = \frac{(P_{\text{BrCl}})^2}{P_{\text{Cl}_2}} = 1 \text{ so, } P_{\text{Cl}_2} = (P_{\text{BrCl}})^2 = 0.01 \text{ atm}$$

then at equilibrium, $\frac{n_{\text{BrCl}}}{n_{\text{Cl}_2}} = \frac{0.1}{0.01} = 10 = \frac{2x}{1-x}$

So, $10 - 10x = 2x$ or $x = \frac{10}{12} = \frac{5}{6}$ moles

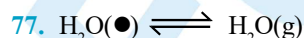
Moles of $\text{Br}_2(\bullet)$ required for maintaining vapour pressure of 0.1 atm

$$= 2 \times \frac{5}{6} \text{ moles} = \frac{10}{6} \text{ moles} = \text{moles of BrCl(g)}.$$

Moles required for taking part in reaction = moles of Cl_2

used up = $\frac{5}{6}$ moles.

Hence total moles required = $\frac{5}{6} + \frac{10}{6} = \frac{15}{6}$ moles.



$$K_p = (P_{\text{H}_2\text{O}})$$

When neon is added at constant pressure, we have to increase volume of the container. So more water will evaporate to maintain equilibrium.

80. $K = A e^{-\Delta H/RT}$

$$\log K = \log A - \frac{\Delta H}{2.303RT}$$

$$\log K = \log A - \frac{\Delta H}{2.303R} \times \frac{1}{T}$$

$$\log K = \left[-\frac{\Delta H}{2.303R} \right] \times \frac{1}{T} + \log A.$$

$$\frac{-\Delta H}{2.303R} = 1.$$

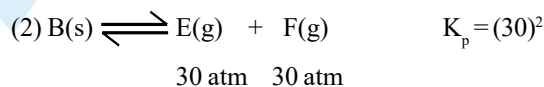
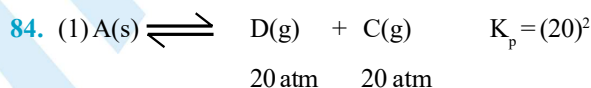
$$\Delta H = -2.303 R = -4.606 \text{ cal.}$$

81. $\log \frac{K_2}{K_1} = \frac{\Delta H^\circ}{2.303R} \left[\frac{1}{T_1} - \frac{1}{T_2} \right]$

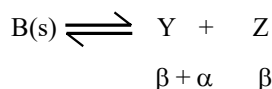
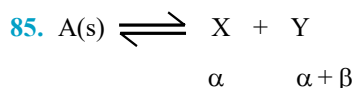
$$\log \frac{K_2}{0.0118} = \frac{597.4 \times 10^3}{2.303 \times 8.314} \left[\frac{1}{1300} - \frac{1}{1200} \right]$$

$$\log K_2 = -2 + \log(0.0118) = -3.928 \Rightarrow K_2 = 1.18 \times 10^{-4}$$

Therefore, (A) option is correct.



(3) container K_p is same so on doubling the volume partial pressure does not change but moles of C, D, E, F will change to maintain their partial pressure. So total pressure = $40 + 60 = 100 \text{ atm}$.



$$\Rightarrow K_{P_1} = \alpha(\alpha + \beta)$$

$$K_{P_2} = \beta(\alpha + \beta)$$

$$P_{\text{total}} = (\alpha + \beta) + \alpha + \beta = 2(\alpha + \beta)$$

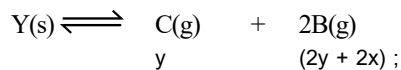
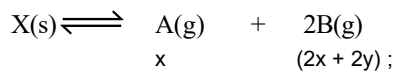
$$\Rightarrow 2(\alpha + \beta) = 50 \Rightarrow \alpha + \beta = 25$$

$$\Rightarrow 250 = 25\alpha \Rightarrow \alpha = 10, \beta = 15$$

$$\Rightarrow K_{P_2} = \beta(\alpha + \beta) = 15 \times 25 = 375$$



87. Let x is partial pressure of A and y is partial pressure of C when both equilibrium simultaneously established in a vessel



$$\frac{K_{P_1}}{K_{P_2}} = \frac{x}{y} \Rightarrow x = 2y$$

$$K_{P_1} = x(2x + 2y)^2$$

$$\Rightarrow x = 0.1 \text{ atm;}$$

$$\therefore y = 0.05 \text{ atm}$$

$$\begin{aligned} \text{Total pressure of gases} &= P_A + P_B + P_C \\ &= 3(x + y) \\ &= 0.45 \text{ atm.} \end{aligned}$$

88. At equilibrium, $r_f = r_b$

$$\therefore K_f[A]_{eq} = K_b[B]_{eq}$$

$$[B]_{eq} = K_f K_b^{-1} [A]_{eq}$$

89. $K = \frac{r_f}{r_b} \Rightarrow 1.5 = \frac{r_f}{7.5 \times 10^{-4}} \Rightarrow r_f = 1.12 \times 10^{-3}$

90. $K_p = \frac{P_{CO(g)} \cdot P_{H_2(g)}}{P_{H_2O(g)}} = \frac{(P_{H_2(g)})^2}{P_{H_2O(g)}} \quad (\text{as } P_{CO(g)} = P_{H_2(g)})$

91. Because reaction is exothermic.

92. Concentration of reactant & product remains const. w.r.t time.

And, rate of [AT EQUILIBRIUM] forward reaction (r_f) = rate of backward reaction (r_b).

93. Equilibrium const. is temp. dependent only.

94. $K_p = K_c (RT)^{\Delta n}$, $\Delta n = 4 - 3 = 1$

$$0.05 = K_c R \times 1000$$

$$K_c = 5 \times 10^{-5} \times R^{-1}$$

95. Since, K_p is temperature dependent only.

96. 4×10^4 , Since Equilibrium const. is temp. dependent only.

EXERCISE - 2

Part # I : Multiple Choice

6. (A) $\Rightarrow [CH_4] = \frac{16}{16 \times 10} = 0.1 \text{ M}$

(B) $\Rightarrow [H_2O] = \frac{18}{18 \times 10} = 0.1 \text{ M}$

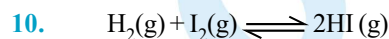
(C) $\Rightarrow [Cl_2] = \frac{35.5}{71 \times 10} = 0.05 \text{ M}$

(D) $\Rightarrow [CO_2] = \frac{44}{44 \times 10} = 0.1 \text{ M}$

7. According to $K_p = \frac{P_{PCl_3(g)} \times P_{Cl_2(g)}}{P_{PCl_5(g)}}$

$$= \frac{(n_{PCl_3(g)})_{eq} \times (n_{Cl_2(g)})_{eq}}{V \times (n_{PCl_5(g)})_{eq}}$$

and on adding inert gas at constant pressure effect on equilibrium will be similar to as if volume of container has been increased.



(A) For changing pressure volume has to be changed, though number of moles of HI(g) do not get changed but its concentration will get changed.

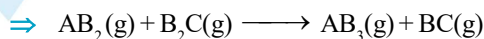
(B) Temperature change will change K_p and hence concentration.

(C) Volume change will change concentration, not the number of moles.

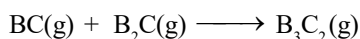
(D) Same equilibrium will be attained from either direction.

(E) Catalyst does not change equilibrium concentrations.

12. Let reactions is started with a mole of AB_2 and b mole of B_2C



a	b	0	0
$a - x$	$b - x - y$	x	$x - y$

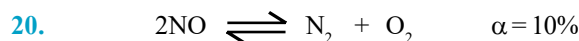


$x - y$	$b - x - y$	y	As $y > x$
---------	-------------	-----	------------

Clearly $[AB_3]_{eq} > [B_3C_2]_{eq}$ and $[AB_3]_{eq} > [BC]_{eq}$

17. Adding inert gas at constant volume does not affect state of equilibrium

19. $N_2 + 3H_2 \rightleftharpoons 2NH_3$ as the reaction is exothermic so more NH_3 will be obtained at lower temperature.



$t = 0$	$4 - .4$	$.2$	$.2$
	3.6	0.2	0.2

$$\Delta n = 0,$$

$$\therefore K_p = K_c, \quad K_c = \frac{(.2/V)^2}{(3.6/V)^2} = \frac{4}{36 \times 36}$$



$$21. \alpha = \frac{D-d}{d} = \frac{46-30}{30} = 0.533 = 53.3\%$$



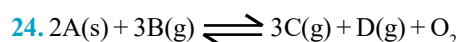
$$M_{Ob} = \frac{M_{th}}{M + (n-1)\alpha} \quad 80 = \frac{100}{1+\alpha} \quad \alpha = \frac{1}{4} = 0.25$$

23. At equilibrium $\Delta G = 0$

$$\text{Given } \Delta G^0 = 0$$

$$\text{Gibbs equation } \Delta G = \Delta G^0 - RT \ln K$$

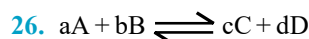
$$0 = 0 - RT \ln K \quad \Rightarrow K = e^0 = 1$$



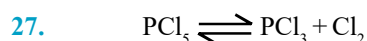
If pressure on system is reduced to half its original value then equilibrium will shift in forward direction to increase no. of moles of gas to compensate reduction of pressure.

\therefore Amounts of C & D will increase.

25. $T \downarrow$, then $V \downarrow$, then $P \uparrow$, equilibrium shift in such direction so as to dec. pressure, i.e., Backward direction.



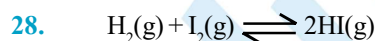
At high temp. & low pressure equilibrium is shifting in backward direction. It means $(a+b) > (c+d)$ & heat will reaction in the formation of producers is $\Delta H < 0$.



$$\begin{array}{lcl} \text{at } t=0 & a & 0 \quad 0 \\ t=tq & a-x & x \quad x \end{array}$$

$$P_{PCl_3} = X_{PCl_3} \times P_T = .25 \times 2 = .5 \text{ atm}$$

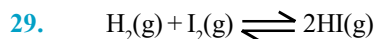
$$P_{PCl_3} = P_{Cl_2} = .5 \text{ atm}$$



$$\begin{array}{lcl} t=0 & 4.5 & 4.5 \quad 0 \\ t=tq. & 4.5-x & 4.5-x \quad 2x \\ \text{put} & x=1.5 & \end{array}$$

$$\begin{array}{lcl} 4.5-1.5 & 4.5-1.5 & 2 \times 1.5 = 3 \\ \downarrow & \downarrow & \downarrow \\ 3 & 3 & 3 \end{array}$$

$$K_c = \frac{(3)^2}{3 \times 3} = 1$$

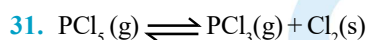


$$\begin{array}{lcl} t=0 & 1.5 & 1.5 \quad 0 \\ t=tev & 1.5-x & 1.5-x \quad 2x \end{array}$$

We know, $1.5-x = 1.25$, or $x = .25$

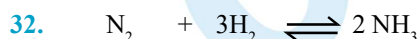
$$K_c = \frac{(.5)^2}{(1.25)^2} = .16$$

30. Since inert gas addition has no effect at const. volume.



at eq, mole of PCl_3 = mole of Cl_2

$$\text{So } K = \frac{[PCl_3][Cl_2]}{[PCl_5]} = \frac{\left[\frac{0.2}{10}\right]\left[\frac{0.2}{10}\right]}{\frac{0.1}{10}} = 0.04$$



$$\begin{array}{lcl} t=0 & 1 \text{ mole} & 2 \text{ mole} \quad 0 \\ t=eq & 1-x & 2-3x \quad 2x=0.8 \\ & & x=0.4 \end{array}$$

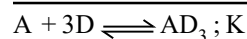
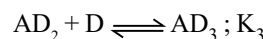
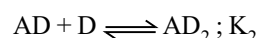
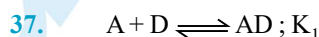
$$\text{mole of } N_2 = 0.6$$

$$\text{mole of } H_2 = 0.8$$



$$\begin{array}{lcl} t=0 & 1 & 1 \quad 1 \quad 0 \\ t=teq & 1-x & 1-x \quad 1+x \quad x \end{array}$$

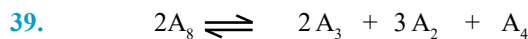
at equilibrium, only CO_2 has $(1+x)$ moles.



As we know that $K = K_1 \cdot K_2 \cdot K_3$

$$\text{Or, } \log K = \log K_1 + \log K_2 + \log K_3$$

$$38. K_p = \frac{(p_{CO})^2}{p_{CO_2}} = \frac{(2)^2}{4} = 1.$$



$$\begin{array}{lcl} t=0 & 2 & 0 \quad 0 \quad 0 \\ t=t_{eq} & 2-2\alpha & 2\alpha \quad 3\alpha \quad \alpha \\ n_T & = 2+4\alpha & \end{array}$$

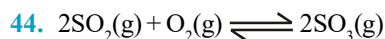
given mole fraction of A_2 is = 0.36.

$$0.36 = \frac{3\alpha}{2+4\alpha}$$

$$\alpha = 0.46$$

$$\text{Mole fraction of } A_8 = \frac{2-2\alpha}{2+4\alpha} = \frac{2-2 \times 0.46}{2+4 \times 0.46} = 0.28$$





$$K_c = \frac{[\text{SO}_3]^2}{[\text{SO}_2]^2[\text{O}_2]}$$

Concentration in gram mole/litre,

therefore

$$[\text{SO}_3] = \frac{48}{80 \times 1}$$

(Where 80 is molecular weight of SO_3)

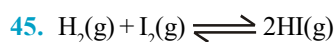
$$[\text{SO}_2] = \frac{128}{64 \times 1}$$

(Where 64 is molecular weight of SO_2)

$$[\text{O}_2] = \frac{9.6}{32 \times 1}$$

(Where 32 is molecular weight of O_2)

$$\text{Thus, } K_c = \frac{\left(\frac{48}{80}\right)^2}{\left(\frac{12.8}{64}\right)^2 \left(\frac{9.6}{32}\right)} = 0.30$$



$$K_c = \frac{[\text{HI}]^2}{[\text{H}_2][\text{I}_2]}$$

if $[\text{H}_2] = [\text{I}_2]$

$$K_c = \frac{[\text{HI}]^2}{[\text{I}_2]^2}$$

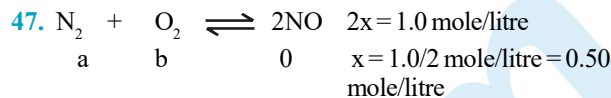
$[\text{HI}]^2 = K_c \times [\text{I}_2]^2$

$$\text{or } \frac{[\text{HI}]^2}{[\text{I}_2]^2} = K_c \quad \text{or } \frac{[\text{HI}]}{[\text{I}_2]} = \sqrt{K_c} = \sqrt{49} = 7$$



Initial mole	1.1	2.2	0	0
At Eq.	1.1 - x	2.2 - 2x	2x	x
	1.1 - 0.1	2.2 - 0.2	0.2	0.1
	1	2	0.2	0.1
Active mass	$\frac{1}{1}$	$\frac{2}{1}$	0.2	0.1

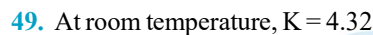
$$K_c = \frac{[\text{C}]^2[\text{D}]}{[\text{A}][\text{B}]^2} = \frac{\frac{2}{10} \times \frac{2}{10} \times \frac{1}{10}}{1 \times 2 \times 2} = \frac{1}{1000} = 0.001$$



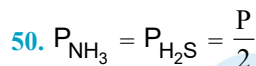
$$(a-x) \quad (b-x) \quad 2x$$

$$\text{If } a-x = 0.25, b-x = 0.05$$

$$[\text{N}_2] = a - x + x = 0.25 + 0.50 = 0.75 \text{ mole/litre}$$



and at 425°C , equilibrium constant become 1.24×10^{-4} i.e. it decreases with increase in temperature. So, it is exothermic reaction.



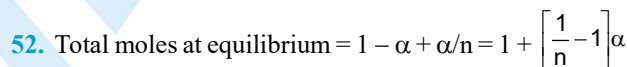
$$\text{Hence } K_p = \text{P}_{\text{NH}_3} \times \text{P}_{\text{H}_2\text{S}} = \frac{P}{2} \times \frac{P}{2} = \frac{P^2}{4}$$



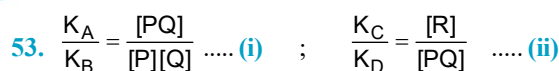
$$\text{Initial conc. } \frac{10^{-3}}{56} \quad b \quad 0$$

$$\text{Final conc. } \frac{10^{-3}}{56} - 6 \times 10^{-6} \quad b - 6 \times 10^{-6} \quad 6 \times 10^{-6}$$

on solving $b = 0.0036 \text{ M}$.

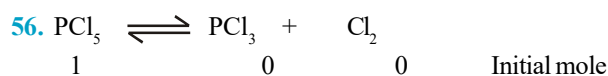
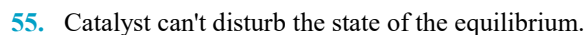


$$\text{So using } \frac{d_i}{d_f} = 1 + \left[\frac{1}{n} - 1\right]\alpha$$



On multiply equation (i) and (ii) we get

$$\frac{K_A \cdot K_C}{K_B \cdot K_D} = \frac{[\text{R}]}{[\text{P}][\text{Q}]}$$



$$\frac{1-0.7}{5} \quad \frac{0.7}{5} \quad \frac{0.7}{5}$$

Conc. at equilibrium

$$\text{Total mole of } \text{PCl}_3 = 0.7$$

$$\text{Concentration} = 0.14$$

$$K_c = \frac{x^2}{(1-x)V} = \frac{0.7 \times 0.7}{0.3 \times 5} = \frac{49}{150}$$



57. K_p depends only on temperature so α will change on changing pressure and $P_{H_2} > P_{N_2}$.

58. $K_p = K_c (RT)^{\Delta n_g} = K_c (RT)$

so, $T = \frac{K_p}{K_c} \cdot \frac{1}{R} = \frac{1}{0.0821} = 12.18 \text{ K}$

59. $K_p = 0.667 \text{ atm} = \frac{2}{3} \text{ atm} = \frac{4\alpha^2}{1-\alpha^2} \cdot P = \frac{4\alpha^2}{1-\alpha^2} \cdot \frac{1}{2}$

so, $\frac{4\alpha^2}{1-\alpha^2} = \frac{4}{3} \Rightarrow 3\alpha^2 = 1 - \alpha^2$

so, $\alpha^2 = \frac{1}{4} \Rightarrow \alpha = \frac{1}{2}$

Part # II : Assertion & Reason

- By definitions.
- Value of equilibrium constant is not dependent on concentration of any species.

EXERCISE - 3

Part # I : Matrix Match Type

- (A) Δn_g is +ve so as P is increased, backward shifting will take place. Total pressure even after shifting will remain same.
(B) Δn_g is -ve so as V is increased, backward shifting will take place. But $P_{\text{final}} < P_{\text{initial}}$.
(C) No change but $P_{\text{final}} < P_{\text{initial}}$ as volume has increased.
(D) Forward shifting will take place and $P_{\text{final}} < P_{\text{initial}}$.

Part # II : Comprehension

Comprehension # 1 :

1. Slope = $\frac{-\Delta H^\circ}{2.3R} = -\frac{230}{2.3 \times 2} = -50$

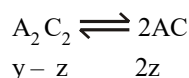
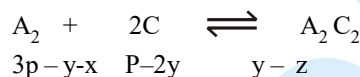
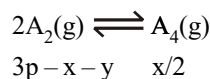
3. Using equation, $\log \frac{K_2}{K_1} = \frac{\Delta H^\circ}{2.30R} \left(\frac{1}{T_1} - \frac{1}{T_2} \right)$

Comprehension # 2 :

- Number of moles will remain unchanged but due to decreased volume pressure will get increased and also the concentrations.

Comprehension # 3 :

Sol. (1 to 3)



$$\frac{P_{A_4}}{P_{A_2}^2} = K_{P_1} \Rightarrow (P_{A_2})^2 = \frac{P_{A_4}}{K_{P_1}} = \frac{\frac{1}{2}}{2/81} = \frac{81}{4}$$

$$\Rightarrow P_{A_2} = \frac{9}{2} \text{ atm.}$$

$$\Rightarrow 3p - x - y = \frac{9}{2} \quad \dots \text{(i)}$$

$$\frac{x}{2} = \frac{1}{2} \quad \dots \text{(ii)}$$

$$\Rightarrow x = 1 \text{ atm}$$

$$\text{also given } 2Z = \frac{1}{2} \quad \dots \text{(iii)}$$

$$Z = \frac{1}{4} \text{ atm}$$

$$P_{\text{total}} = 3p - x - y + x/2 + p - 2y + y - z + 2z = 4p - x/2 - 2y + z$$

$$= 4 \times p - \frac{1}{2} - 2 \times \frac{1}{2} + \frac{1}{4} = \frac{27}{4} \text{ atm.} \Rightarrow P = 2 \text{ atm.}$$

Sol.1 $3P - x - y = \frac{9}{2}$

$$6 - \frac{1}{2} - y = \frac{9}{2}$$

$$y = 1 \text{ atm.}$$

$$P_{A_2C_2} = y - z = 1 - \frac{1}{4} = \frac{3}{4} \text{ atm.}$$

Sol.2 $\frac{n_{A_2}}{n_{AC}} = \frac{P_{A_2}}{P_{AC}} = \frac{3P - x - y}{2z} = \frac{\frac{9}{2}}{1/2} = 9$

Sol.3 $K_p = \frac{P_{A_2C_2}}{P_{AC}^2} = \frac{3/4}{\left(\frac{1}{2}\right)^2} = 3$



Comprehension # 5 :



$$\Delta H^\circ = \frac{3}{2} (-241.8) + (-1575) - (-2021)$$

$$\text{For 1 kg CaSO}_4 \cdot 2\text{H}_2\text{O} = \frac{\Delta H^\circ}{172} \times 100 = 484 \text{ kJ}$$

2. $\Delta S^\circ = \frac{3}{2} (188.6) + 130.5 - 194$

$$\Delta G^\circ = \Delta H^\circ - (298) \Delta S^\circ = -8.314 \times 298 \ln (P_{\text{H}_2\text{O}})^{3/2}$$

$$\Rightarrow P_{\text{H}_2\text{O}} = 8.1 \times 10^{-3} \text{ bar}$$

EXERCISE - 4
Subjective Type

2. $n = \frac{5.6}{22.4} = 0.25$

$$\text{Active mass} = \frac{0.25}{5.6} = 0.044 \text{ M.}$$

5. Forward reaction rate (r_f) = $K_1 [\text{A}] [\text{B}]$

Backward reaction rate (r_b) = $K_2 [\text{C}] [\text{D}]$

At equilibrium, $r_f = r_b$

$$\therefore K_1 [\text{A}] [\text{B}] = K_2 [\text{C}] [\text{D}]$$

The concentration of reactants & products at equilibrium are related by

$$K = \frac{K_1}{K_2} = \frac{[\text{C}] [\text{D}]}{[\text{A}] [\text{B}]}$$

$$\therefore K = \frac{K_1}{K_2}$$

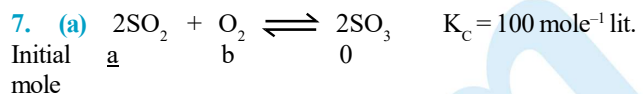


No. of mole 2 1 4

conc. $\frac{2}{4}$ $\frac{1}{4}$ $\frac{4}{4}$

$$K_c = \frac{[\text{SO}_3]}{[\text{SO}_2][\text{O}_2]^{1/2}} = \frac{1}{(1/2)(1/4)^{1/2}}$$

$$= \frac{1}{(1/2) \times (1/2)} = 4 \text{ Ans.}$$



Initial
mole

$$a-2x \quad b-x \quad 2x$$

$$\frac{a}{2} \quad b - \frac{a}{4} \quad \frac{a}{2} \quad (\text{According to data given})$$

But according to question.

$$\text{No. of mole of SO}_2 = \text{No. of mole of SO}_3$$

$$= a - 2x = 2x.$$

$$a = 4x.$$

$$x = \frac{a}{4}.$$

$$\text{Now, } K_c = \frac{[\text{SO}_3]^2}{[\text{SO}_2]^2 [\text{O}_2]}$$

But No. of mole of SO_3 and SO_2 are equal at eq. so.

$$K_c = \frac{1}{[\text{O}_2]}$$

$$[\text{O}_2] = \frac{1}{K_c}; \quad [\text{O}_2] = \frac{1}{100}.$$

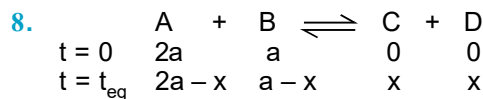
$$\text{But } [\text{O}_2] = \frac{\text{mole of O}_2 \text{ at eq.}}{10} = \frac{1}{100}.$$

$$\text{So No. of mole of O}_2 = \frac{1}{10} = 0.1.$$

$$(b) K_c = \frac{[\text{SO}_3]^2}{[\text{SO}_2]^2 [\text{O}_2]} = \frac{\left(\frac{2n_{\text{SO}_2}}{V}\right)^2}{\left(\frac{n_{\text{SO}_2}}{V}\right)^2 \times \left(\frac{n_{\text{O}_2}}{V}\right)}$$

$$K_c = \frac{4}{\left(\frac{n_{\text{O}_2}}{V}\right)};$$

$$n_{\text{O}_2} = \frac{4 \times V}{K_c} = \frac{4 \times 10}{100} = 0.4.$$



$$t = 0 \quad 2a \quad a \quad 0 \quad 0$$

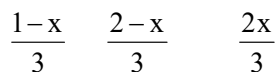
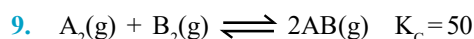
$$t = t_{\text{eq}} \quad 2a - x \quad a - x \quad x \quad x$$

$$a - x = x \Rightarrow x = \frac{a}{2}$$

$$\Rightarrow K_c = \frac{\frac{a}{2} \times \frac{a}{2}}{\left(2a - \frac{a}{2}\right) \times \frac{a}{2}} = \frac{1}{3} \Rightarrow \frac{1}{K_c} = 3$$

Ans. 3

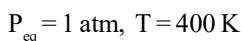
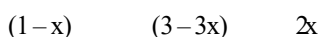
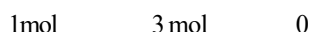
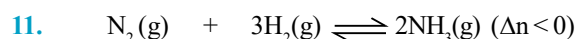




$$50 = \frac{\frac{2x}{3} \cdot \frac{2x}{3}}{\frac{1-x}{3} \cdot \frac{2-x}{3}} = \frac{4x^2}{(1-x)(2-x)} = \frac{4x^2}{2-3x+x^2}$$

$$\Rightarrow 100 - 150x + 50x^2 = 4x^2$$

$$\therefore \text{no. of mol of AB} = \frac{2x}{3} = 1.868.$$



$$K_c = \frac{[NH_3]^2}{[N_2][H_2]^3} = \frac{(2x)^2}{(1-x)(3-3x)^3} = \frac{4}{27}$$

$$\frac{x^2}{(1-x)^4} = 1 \Rightarrow x = (1-x)^2 \Rightarrow x^2 - 3x + 1 = 0$$

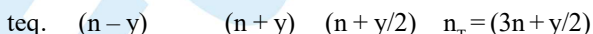
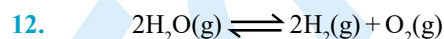
$$\Rightarrow x = \frac{3 \pm \sqrt{9-4}}{2} \Rightarrow x = \frac{3 \pm \sqrt{5}}{2}$$

$$x = \frac{3+2.24}{2} \text{ or } x = \frac{3-2.24}{2}$$

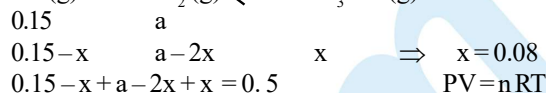
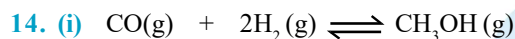
$$x = \frac{5.24}{2} = 2.62 \text{ or } x = \frac{0.76}{2}$$

$$\Rightarrow x = 0.38 \text{ (since } x \text{ cannot be greater than 1)}$$

$$\therefore [NH_3] = 0.38 \times 2 = 0.76$$



$$\text{so, } K_p = \frac{(P_{H_2(g)})_{eq.}^2 \cdot (P_{O_2(g)})_{eq.}}{(P_{H_2O(g)})_{eq.}^2} = \frac{(n+y)^2 (n+y/2) P}{(n-y)^2 (3n+y/2)}$$

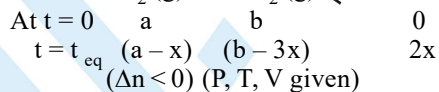


$$a-2x = 0.35 \quad n = \frac{8.2 \times 2.5}{0.082 \times 500} = 0.5$$

$$K_c = \frac{0.08}{\frac{0.07}{2.5} \times \left(\frac{0.35}{2.5}\right)^2} = \frac{20000}{343} = 58.3$$

$$K_p = 58.3 \times (RT)^{-2} = \frac{58.3}{(0.082 \times 500)^2} = \frac{58.3}{41 \times 41} = 0.035$$

(ii) Total pressure will remain 8.2 atm as catalyst reduces only time taken to achieve equilibrium, does not affect equilibrium condition / concentrations.



$$[N_2] = \frac{a-x}{V}, \quad [H_2] = \frac{b-3x}{V}, \quad [NH_3] = \frac{2x}{V}$$

$$K_c = \frac{\left(\frac{2x}{V}\right)^2}{\left(\frac{a-x}{V}\right)\left(\frac{b-3x}{V}\right)^3} = \frac{4x^2 V^2}{(a-x)(b-3x)^3}$$

$$\text{Total no. of moles at equilibrium} = a + b - 2x$$

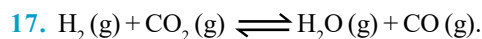
$$[P_{N_2}] = \frac{(a-x)}{a+b-2x} \cdot P, \quad [P_{H_2}] = \frac{(b-3x)}{a+b-2x} \cdot P,$$

$$[P_{NH_3}] = \frac{(2x) \cdot P}{a+b-2x}$$

$$\therefore K_p = \frac{[P_{NH_3}]^2}{[P_{N_2}][P_{H_2}]^3}$$

$$= \frac{\left(\frac{2x}{a+b-2x} \cdot P\right)^2}{\left[\left(\frac{a-x}{a+b-2x}\right) \cdot P\right] \left[\left(\frac{b-3x}{a+b-2x}\right) \cdot P\right]^3}$$

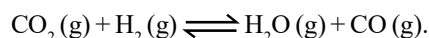
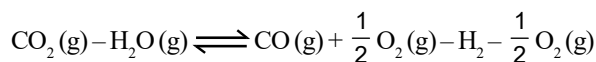
$$K_p = \frac{4x^2 \cdot P^2}{P^4 \cdot \frac{(a-x)(b-3x)^3}{(a+b-2x)^4}} = \frac{(a+b-2x)^2 \cdot 4x^2}{P^2 (a-x)(b-3x)^3}$$



$$2\text{H}_2\text{O}(\text{g}) \rightleftharpoons 2\text{H}_2(\text{g}) + \text{O}_2(\text{g}) \quad K_1 = 2.1 \times 10^{-13} \quad \dots(1)$$

$$2\text{CO}_2(\text{g}) \rightleftharpoons 2\text{CO}(\text{g}) + \text{O}_2(\text{g}) \quad K_2 = 1.4 \times 10^{-12} \quad \dots(2)$$

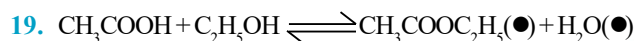
$$\frac{1}{2} \text{ eq. (2)} - \frac{1}{2} \text{ eq. (1)}$$



$$\frac{1}{2} [\text{eq. (2)} - \text{eq. (1)}]$$

$$K = \left(\frac{K_2}{K_1} \right)^{1/2} = \left(\frac{1.4 \times 10^{-12}}{2.1 \times 10^{-13}} \right)^{1/2} = \left(\frac{14}{2.1} \right)^{1/2}$$

= 2.58. Ans.



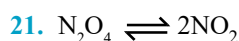
Initial	1	1	0	1
At eq.	1-x	1-x	x	1+x
	1-0.543	1-0.543	0.543	1+0.543

$$(54.3\% \text{ of } 1 \text{ mole}) = \frac{1 \times 54.3}{100} = 0.543 \text{ mole}$$

Hence given x = 0.543 mole

Applying law of mass action :

$$K_c = \frac{[\text{ester}][\text{water}]}{[\text{acid}][\text{alcohol}]} = \frac{0.543 \times 1.543}{0.457 \times 0.457} = 4.0$$



1	0
1-.25	.50
.75	.50

$$n_{\text{total}} = 1.25$$

$$P_{\text{N}_2\text{O}_4} = \left(\frac{.75}{1.25} \right); \quad P_{\text{NO}_2} = \left(\frac{.50}{1.25} \right)$$

$$K_p = \frac{(P_{\text{NO}_2})^2}{(P_{\text{N}_2\text{O}_4})} = \frac{(.50/1.25)^2}{(.75/1.25)} = \frac{.50 \times .50}{1.25 \times .75}$$

$$= \frac{4}{15} = 0.266.$$

At pressure 0.1 atm,



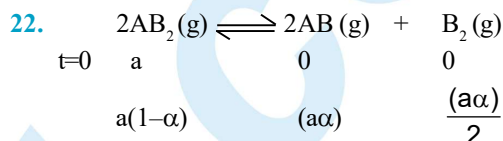
1	0
(1-α)	2α

$$P_{\text{N}_2\text{O}_4} = \left(\frac{1-\alpha}{1+\alpha} \right) \times 0.1; \quad P_{\text{NO}_2} = \left(\frac{2\alpha}{1+\alpha} \right) \times 0.1$$

$$K_p = \frac{\left(\frac{2\alpha}{1+\alpha} \times 0.1 \right)^2}{\left(\frac{1-\alpha}{1+\alpha} \right) \times 0.1}; \quad K_p = \frac{4\alpha^2 \times 0.1}{(1+\alpha)(1-\alpha)}$$

$$0.266 = \frac{0.1 \times 4\alpha^2}{1-\alpha^2}$$

$$0.665 = (1+0.665)\alpha^2. \Rightarrow \alpha = 63.25\%.$$



$$\text{Total mole} = a[1-\alpha+\alpha+\frac{\alpha}{2}] = \frac{a[2+\alpha]}{2}$$

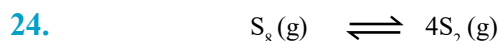
$$P_{\text{AB}_2} = \frac{a(1-\alpha) \times 2}{a(2+\alpha)} \times P; \quad P_{\text{AB}} = \frac{a\alpha \times 2}{a(2+\alpha)} \times P$$

$$P_{\text{B}_2} = \frac{\left(\frac{a\alpha}{2} \right)}{a(2+\alpha)} = \left[\frac{\alpha}{2+\alpha} \right] \times P.$$

$$K_p = \frac{\left(\frac{2\alpha}{2+\alpha} \times P \right)^2 \left(\frac{\alpha}{2+\alpha} \times P \right)}{\left(\frac{2(1-\alpha)}{2+P} \times P \right)^2}$$

$$\alpha \ll 1.$$

$$K_p = \frac{\alpha^3 P}{2}; \quad \alpha = \left(\frac{2K_p}{P} \right)^{1/3} \text{ i.e. } x = \left(\frac{2K_p}{P} \right)^{1/3}$$



time t=0	1 atm	0
At. eq.	(1-x)	4x

$$\text{Pressure of eq.} \quad 1-0.29 \quad 4 \times 0.29.$$

$$K_p = \frac{(P_{\text{S}_2})^4}{P_{\text{S}_8}} = \frac{(4 \times 0.29)^4}{0.71}$$

$$K_p = 2.55 \text{ atm}^3.$$

26.
$$\begin{array}{ccccccc} \text{C(s)} & + & \text{H}_2\text{O(g)} & \rightleftharpoons & \text{CO(g)} & + & \text{H}_2\text{(g)} \\ t=0 & & - & & 1 & & 2 & & 3 \\ & & & & & & & & \end{array}$$

carbon solid will start forming when there will be equilibrium in the container

$$K_p = \frac{P_{\text{CO}} \cdot P_{\text{H}_2}}{P_{\text{H}_2\text{O}}} = 3 \text{ atm} = \frac{(2P)(3P)}{P} = 6P = 3 \text{ atm}$$

So $P = \frac{1}{2} \text{ atm}$

So Total pressure in the container will be

$$P_T = P + 2P + 3P = 6P = 3 \text{ atm} \quad \text{Ans. 3}$$

28.
$$\begin{array}{ccccccc} \text{SO}_2\text{(g)} & + & \text{NO}_2\text{(g)} & \rightleftharpoons & \text{NO(g)} & + & \text{SO}_3\text{(g)} \\ 0.04 & & 0.04 & & 0.3 & & 0.3 \\ 0.04-x & & 0.04-x & & 0.3+x & & 0.3+x \end{array}$$

$$Q_c = \frac{(0.3)^2}{(0.04)^2} = 56.25$$

Here, $Q_c < K_c$ hence reaction will proceed in forward direction to reach at state of equilibrium

$$K_c = \frac{(0.3+x)^2}{(0.04-x)^2} = 81$$

$$x = 0.006$$

30. Equation (iii) = $-[2 \times \text{(i)} + \text{(ii)}]$

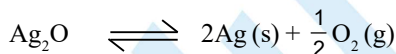
$$\therefore K_{2000} \text{ (iii)} = \frac{1}{K_1^2 K_2} = \frac{1}{(4.4)^2 \times 5.31 \times 10^{-10}} = 9.7 \times 10^7$$

$\ominus T \uparrow K \downarrow \Rightarrow$ reaction is exothermic.

31. $T = 445^\circ\text{C} = 445 + 273 = 718\text{K}$

$$P = 207 \text{ atm}$$

$$n = 1 \text{ mole}$$



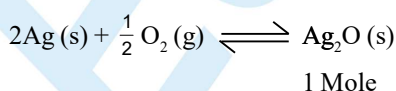
$$K_p = \sqrt{P_{\text{O}_2}} = (207)^{1/2} = 14.39$$

$$\Delta G^0 = \Delta G^0 + 2.303 RT \log K_{\text{eq}}$$

But at eq. $\Delta G = 0$,

$$\Delta G^0 = -2.303 RT \log K_{\text{eq}}$$

But for formation,



$$K_p = \frac{1}{(P_{\text{O}_2})^{1/2}} = \frac{1}{(207)^{1/2}}$$

$$\Delta G^0 = -2.303 \times 8.312 \times 718 \log \frac{1}{(207)^{1/2}}$$

$$\Delta G^0 = \frac{2.303 \times 8.312 \times 718}{2} \times \log 207$$

$$\Delta G^0 = 6872.17 \log 207$$

$$\Delta G^0 = 15915.75 \text{ J}$$

$$\Delta G^0 = 3789.46 \text{ Cal}$$

$$\Delta G^0 = 3.789 \text{ KCal}$$

$$\Delta G^0 = 3.8 \text{ KCal}$$

33.
$$\text{SrCl}_2 \cdot 6\text{H}_2\text{O(s)} \rightleftharpoons \text{SrCl}_2 \cdot 2\text{H}_2\text{O(s)} + 4\text{H}_2\text{O(g)}$$

 $K_p = 16 \times 10^{-12}$

$$(P_{\text{H}_2\text{O}})^4 = K_p \quad P_{\text{H}_2\text{O}} = (K_p)^{1/4} = 2 \times 10^{-3} \text{ atm}$$

$$\text{H}_2\text{O(l)} \rightleftharpoons \text{H}_2\text{O(g)} \quad P_{\text{H}_2\text{O}} = \frac{7.6}{760} = 1.0 \times 10^{-2}$$

$$n_{\text{H}_2\text{O}} = \frac{PV}{RT} = \frac{10^{-2} \times 1}{0.082 \times 274} = 4.45 \times 10^{-4}$$

$$n_{\text{H}_2\text{O}} = \frac{2 \times 10^{-3}}{0.082 \times 274} = 8.9 \times 10^{-5}$$

$$\therefore n_{\text{H}_2\text{O}} \text{ absorbed} = 3.56 \times 10^{-4}$$

$$\therefore \text{wt absorbed} = 6.4 \text{ mg.}$$

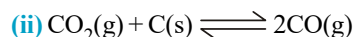
$$36. \text{ (a)} K_p = \frac{P_{\text{CO}} \times P_{\text{H}_2}^3}{P_{\text{CH}_4} \times P_{\text{H}_2\text{O}}}$$

(b) (i) The value of K_p remains unchanged on increasing the pressure. When pressure is increased then according to Le-Chatelier's principle the equilibrium shifts in the direction where there is less number of moles of gases i.e., backward direction in case of the given reaction.

(ii) In case of endothermic reactions the value of K_p increases with increases in temperature. With increases in temperature, the equilibrium shift in the endothermic direction i.e., forward direction in case of the given reaction.

(iii) K_p will remain undisturbed. Equilibrium composition will remain unchanged. However, in the presence of catalyst, the equilibrium would be attained quickly.

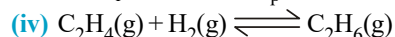
- 37.. (i) In this case n_p is equal to n_r
This reaction will not be affected by increase of pressure.



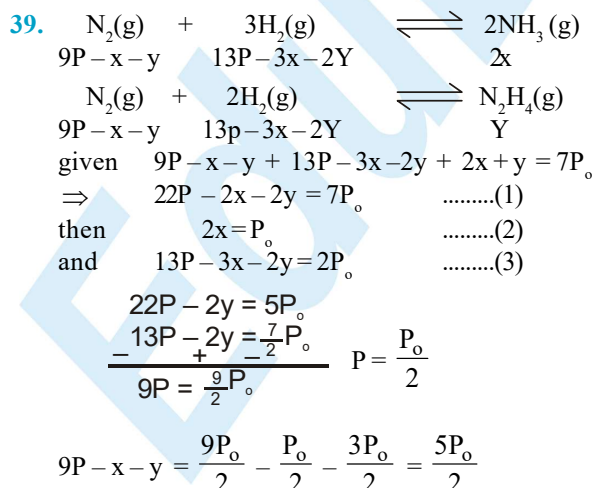
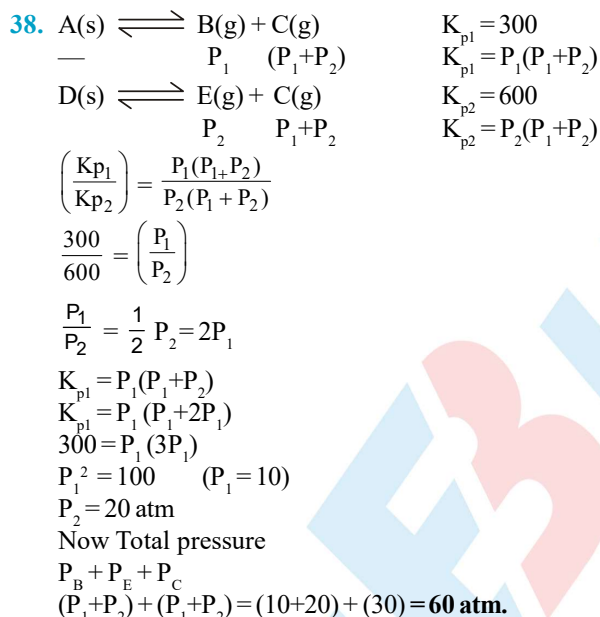
In this reaction, moles of gases on product side ($n_p = 2$) is more than that on reactant side ($n_r = 1$). This reaction **will be affected** by increase in pressure. Increase in pressure shifts the equilibrium in that direction where there is less no. of moles gases. In this reaction, increase in pressure will cause the reaction to go into the **left direction**.



The reaction **would be affected** by increase in pressure because n_p is different from n_r . Increase in pressure shifts the equilibrium in **left direction** because n_r is less than n_p .



The reaction **would be affected** by increase in pressure. Increase in pressure will shift the equilibrium **towards right** because n_p is less than n_r .



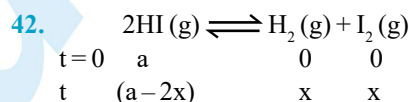
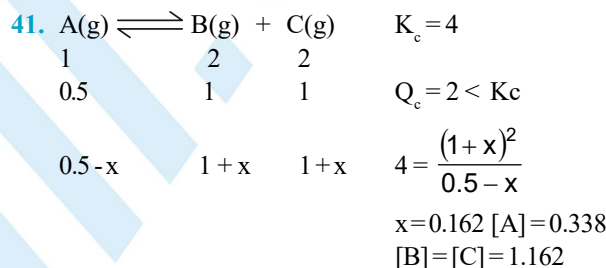
$$2y = \frac{13 - 7}{2} P_0 = 3P_0$$

$$13P - 3x - 2y = \frac{13P_0}{2} - \frac{3P_0}{2} - \frac{6P_0}{2} = 2P_0 \quad y = \frac{3}{2} P_0$$

$$K_1 = \frac{(2x)^2}{(9P - x - y)(13P - 3x - 2y)^3}$$

$$= \frac{P_0^2}{\frac{5}{2}P_0 \cdot (2P_0)^3} = \frac{1}{20P_0^2}$$

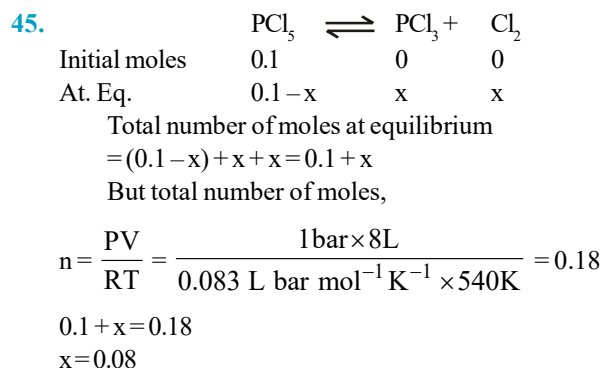
$$K_2 = \frac{\frac{3}{2}P_0}{\left(\frac{5}{2}P_0\right)(2P_0)^2} = \frac{3}{20P_0^2}$$



$$\text{Given: } \frac{x^2}{(a-2x)^2} = \frac{1}{54.8}$$

$$\text{so, } \frac{a-2x}{x} = \sqrt{54.8} \text{ and } (a-2x) = 0.5 \text{ M}$$

$$\text{so, } x = \frac{0.5}{\sqrt{54.8}} = \frac{0.5}{7.40} = 0.0675 \text{ M}$$



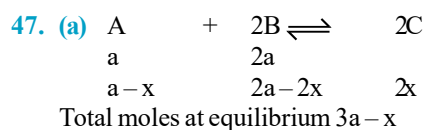
$$[\text{PCl}_5] = \frac{0.1 - 0.08}{8} \text{ M} = 2.5 \times 10^{-3} \text{ M}$$

$$[\text{PCl}_3] = \frac{0.08}{8} \text{ M} = 0.01 \text{ M}$$

$$[\text{Cl}_2] = \frac{0.08}{8} \text{ M} = 0.01 \text{ M}$$

$$K_c = \frac{[\text{PCl}_3][\text{Cl}_2]}{[\text{PCl}_5]} = \frac{0.01 \times 0.01}{2.5 \times 10^{-3}} = 4 \times 10^{-2}$$

$$K_p = K_c (RT)^{\Delta n} = 4 \times 10^{-2} \times (0.083 \times 540) = 1.79 \text{ bar}$$



Total moles at equilibrium $3a - x$

$$\text{Mole fraction of C} = \frac{2x}{3a - x} = 0.4$$

$$2x = 1.2a - 0.4x$$

$$x = \frac{1.2a}{2.4}$$

$$x = \frac{a}{2}$$



$$\text{Total moles} = \frac{5a}{2}$$

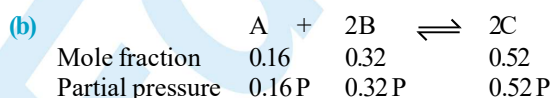
$$P_A = \frac{\frac{a}{2}}{\frac{5a}{2}} \times 8 = \frac{8}{5} \text{ atm}$$

$$P_B = \frac{a}{5a/2} \times 8 = \frac{16}{5} \text{ atm}$$

$$P_C = \frac{a}{5a/2} \times 8 = \frac{16}{5} \text{ atm}$$

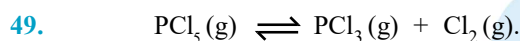
$$K_p = \frac{(P_C)^2}{(P_B)^2 \cdot P_A} = \frac{5}{8}$$

$$K_p = 0.625 \text{ atm}^{-1}$$



$$K_p = \frac{(0.52P)^2}{0.16P \times (0.32P)^2} = \frac{5}{8}$$

$$P = \frac{0.52 \times 0.52 \times 8}{0.16 \times 0.32 \times 0.32 \times 5} = 26.4 \text{ atm}$$



Initial total moles = (3+1) = 4.

Now from Ideal gas equation

$$PV = nRT = P \times 100 = 4 \times 0.082 \times 500$$

$$P = 0.082 \times 20 = 1.64 \text{ atm.}$$

At equilibrium Total mole = $3 - x + x + 1 + x = (4 + x)$

$$PV = nRT.$$

$$2.05 \times 100 = (4+x) \times 0.082 \times 500.$$

$$2.05 = (4+x) \times 0.41.$$

$$5 = 4 + x.$$

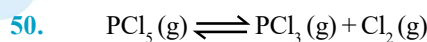
$$x = 1.$$

$$\alpha = \frac{\text{No. of mole dissociated}}{\text{Initially total mole taken}} = \frac{1}{3} = 0.33.$$

$$P_{\text{PCl}_5} = \frac{2}{5} \times 2.05; \quad P_{\text{PCl}_3} = \frac{1}{5} \times 2.05$$

$$P_{\text{Cl}_2} = \frac{2}{5} \times 2.05$$

$$K_p = \frac{\left(\frac{1}{5} \times 2.05\right) \left(\frac{2}{5} \times 2.05\right)}{\left(\frac{2}{5} \times 2.05\right)} = [0.41]$$



$$\text{Given, } (1 \text{ atm})(2.05 \text{ L}) = \left(\frac{8.34}{208.5} + x \text{ mole}\right) (0.082 \text{ L}$$

$$\text{atm mole}^{-1} \text{ K}^{-1}) (500 \text{ K})$$

$$\text{so, } \frac{8.34}{208.5} + x = \frac{2.05}{0.082 \times 500} = 0.05 \text{ mole}$$

$$x = 0.05 - 0.04 = 0.01$$

$$\text{so, } \alpha = \frac{0.01}{0.04} = 0.25 = 25\%$$

$$K_p = \frac{\alpha^2}{1 - \alpha^2} \cdot P = \left(\frac{1/16}{1 - (1/16)}\right) = \frac{1}{15} \text{ atm.}$$

52. $\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ$; $K = e^{-\Delta G^\circ / RT}$

At 300 K, $\Delta G^\circ = [(-41.16) - (300 \times -0.0424)] \times 1000$
 $= -28440 \text{ J/mol} = -RT \ln K_p$

At 1200 K, $\Delta G^\circ = [(-32.93) - (1200 \times -0.0296)] \times 1000$
 $= +2590 \text{ J/mol} = -RT \ln K_p$

$K_p(300 \text{ K}) = 8.935 \times 10^4$

$K_p(1200 \text{ K}) = 0.7753$

$Q = 1$

at 300 K: $Q < K$, Hence forward direction.

at 1200 K: $Q > K$, Hence backward direction.

53. (i) $\text{N}_2\text{O}_4 \rightleftharpoons 2\text{NO}_2$; $G^\circ_{\text{N}_2\text{O}_4} = 100 \text{ kJ mol}^{-1}$

conc. at $t = 0$ 5 5 $G^\circ_{\text{N}_2\text{O}_4} = 50 \text{ kJ mol}^{-1}$

$\Delta G^\circ \text{ for reaction} = 2 \times G^\circ_{\text{N}_2\text{O}_4} - G^\circ_{\text{N}_2\text{O}_4} = 2 \times 50 - 100 = 0$

Now, $\Delta G = \Delta G^\circ + 2.303 RT \log Q$

$\Delta G = 0 + 2.303 \times 8.314 \times 10^{-3} \times 298 \log \frac{5^2}{5} = +3.99 \text{ kJ}$

(ii) Since ΔG is +ve and thus reaction will not proceed in forward direction.

Also for reverse reaction:



Mole at $t=0$ 5 5

Mole at eq. $(5-2x)$ $(5+x)$

$\therefore \Delta G = -2.303 RT \log K_c$

$\therefore \Delta G^\circ = 0 \quad \therefore K_c = 1$

or $1 = \frac{5+x}{(5-2x)^2}$

$\therefore x = 1.25$

Thus, $[\text{NO}_2]_{\text{at eq.}} = 5 - 2.5 = 2.5$

$[\text{N}_2\text{O}_4]_{\text{at eq.}} = 5 + 1.25 = 6.25$

56. $\text{N}_2\text{O}_4 \rightleftharpoons 2\text{NO}_2(\text{g})$ $d_{\text{mix}} = \frac{PM_{\text{mix}}}{RT}$

$M_{\text{mix}} = \frac{1.8 \times 0.082 \times 346}{1} = 51.0696$

$1 - \alpha \quad 2\alpha \quad M_{\text{mix}} = 51.0696$
 $0.2 \quad 0.8 \times 2 = 1.6$

$M_{\text{mix}} = \frac{92}{1+\alpha} \quad 1+\alpha = \frac{92}{51} \quad \alpha = 0.8$

$K_p = \frac{\left(\frac{1.6}{1.8} \times 1\right)^2}{\left(\frac{0.2}{1.8} \times 1\right)} = 7.11 \quad K_p = K_c RT \quad K_c = \frac{K_p}{RT}$

$K_c = \frac{7.11}{0.082 \times 346} = 0.25$

58. $\text{SO}_2(\text{g}) + \text{NO}_2(\text{g}) \rightleftharpoons \text{SO}_3(\text{g}) + \text{NO}(\text{g})$

Suppose x moles of SO_2 react with x moles of NO_2 to form x moles of SO_3 and x moles of NO to attain equilibrium. The equilibrium concentration, therefore would be

$[\text{SO}_2] = (1-x) \text{ mol L}^{-1}; \quad [\text{NO}_2] = (1-x) \text{ mol L}^{-1};$

$[\text{SO}_3] = (1+x) \text{ mole L}^{-1}; \quad [\text{NO}] = (1+x) \text{ mole L}^{-1}$

$K_c = \frac{[\text{SO}_3][\text{NO}]}{[\text{SO}_2][\text{NO}_2]} = \frac{(1+x)(1+x)}{(1-x)(1-x)} = 16$

$\frac{(1+x)^2}{(1-x)^2} = 16 \quad \text{or} \quad \frac{(1+x)}{(1-x)} = 4$

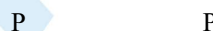
$1+x = 4-4x \quad \text{or} \quad 5x = 3$

or $x = \frac{3}{5} = 0.6 \text{ mole}$

$[\text{NO}_2] = (1-x) = (1-0.6) = 0.4 \text{ mol L}^{-1}$

$[\text{NO}] = (1+x) = (1+0.6) = 1.6 \text{ mol L}^{-1}$

59. $\text{Ni}(\text{s}) + 4\text{CO}(\text{g}) \rightleftharpoons \text{Ni}(\text{CO})_4(\text{g})$



For backward reaction

$Q_p \geq K_p$

$\frac{P}{P^4} \geq K_p$

$\therefore \frac{1}{P^3} \geq 0.125 \text{ atm}^{-3}$

$P^3 \leq 8 \text{ atm}^3$

$P \leq 2 \text{ atm}$

$P_{\text{Total}} = 2P = 4 \text{ atm}$

60. $\text{A}(\text{s}) \rightleftharpoons \text{A}'(\text{g}) + \text{H}_2\text{S}(\text{g})$



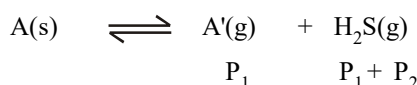
$P = 50 \text{ mm} \Rightarrow P_{\text{H}_2\text{S}} = P_{\text{A}'} = P/2 = 25 \text{ mm}$

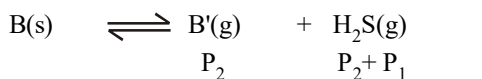


$P = 68 \text{ mm} \Rightarrow P_{\text{H}_2\text{S}} = P_{\text{B}'} = P/2 = 34 \text{ mm}$

(i) $K_{p_1} = (25)^2 = 625 \text{ mm}^2$; $K_{p_2} = (34)^2 = 1156 \text{ mm}^2$

(ii) Ratio of moles is same as that of partial pressure so,





$$K_{P_1} = P_A \times P_{\text{H}_2\text{S}} = P_1(P_1 + P_2) \quad \dots\dots\dots \text{(i)}$$

$$K_{P_2} = P_{\text{B'}} \times P_{\text{H}_2\text{S}} = P_2(P_1 + P_2) \quad \dots\dots\dots \text{(ii)}$$

$$\frac{K_{P_1}}{K_{P_2}} = \frac{P_1}{P_2} = \frac{625}{1156}$$

$$\text{(iii) total pressure} = P_1 + P_2 + (P_1 + P_2) = 2(P_1 + P_2)$$

$$\text{(i) + (ii)} = (P_1 + P_2)^2$$

$$\sqrt{K_{P_1} + K_{P_2}} = P_1 + P_2$$

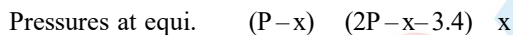
$$P_T = 2 \times (\sqrt{K_{P_1} + K_{P_2}}) = 84.4 \text{ mm.}$$

61. For I equilibrium $2\text{NO}_2 \rightleftharpoons \text{N}_2\text{O}_4$

$$K_p = \frac{P_{\text{N}_2\text{O}_4}}{(P_{\text{N}_2\text{O}_4})^2} = 6.8 \quad \dots\dots\dots \text{(1)}$$

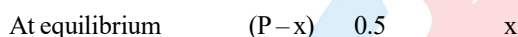
→ $P_{\text{N}_2\text{O}_4} = 1.7 \text{ atm}$ ∴ By Eq. (1); $P_{\text{NO}_2} = 0.5 \text{ atm}$

The equilibria are maintained using NO and NO₂ in the ratio 1 : 2



→ 3.4 atm of NO₂ are used for I equilibrium to have

$$P_{\text{N}_2\text{O}_4} = 1.7 \text{ atm}$$



(→ P_{NO_2} is same for both the equilibria since both reactions are at equilibrium at a time.)

Total pressure at equilibrium (Given 5.05 atm)

$$= P_{\text{NO}} + P_{\text{NO}_2} + P_{\text{N}_2\text{O}_3} + P_{\text{N}_2\text{O}_4}$$

$$= P - x + 0.5 + x + 1.7$$

$$\therefore 5.05 = P + 2.20$$

$$\therefore P = 5.05 - 2.20$$

$$\therefore P = 2.85 \text{ atm}$$

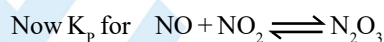
$$\rightarrow 2P - x - 3.4 = 0.5$$

$$2 \times 2.85 - x - 3.4 = 0.5$$

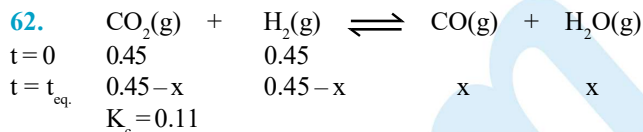
$$\therefore x = 5.70 - 3.90$$

$$\therefore x = 1.80 \text{ atm}$$

$$\therefore P_{\text{NO}} = 2.85 - 1.80 = 1.05 \text{ atm}$$

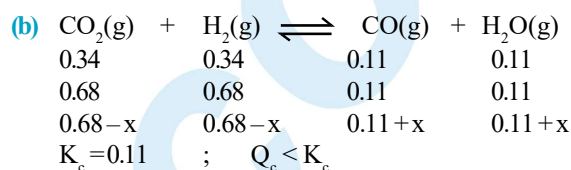


$$K_p = \frac{P_{\text{N}_2\text{O}_3}}{P_{\text{NO}} \times P_{\text{NO}_2}} = \frac{1.80}{1.05 \times 0.5} = 3.43 \text{ atm}^{-1}$$



$$0.11 = \left(\frac{x/v}{0.45-x} \right)^2 \quad \frac{x}{0.45-x} = 0.33 \quad x = 0.11$$

$$\text{(a) } n_{\text{CO}} = n_{\text{H}_2\text{O}} = 0.11 \quad n_{\text{CO}_2} = n_{\text{H}_2} = 0.34$$



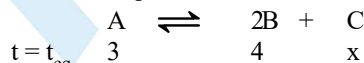
$$0.11 = \left(\frac{0.11+x}{0.68-x} \right)^2 \quad \frac{0.11+x}{0.68-x} = 0.33 = \frac{1}{3}$$

$$0.33 + 3x = 0.68 - x$$

$$4x = 0.35 \quad x = 0.0875 \quad n_{\text{CO}} = n_{\text{H}_2\text{O}} = 0.1975$$

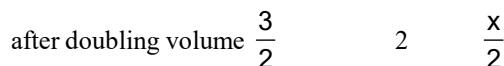
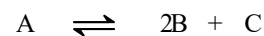
$$n_{\text{CO}_2} = n_{\text{H}_2} = 0.5925$$

63. Let initial equilibrium concentration of C = x M



$$K_C = \frac{x \times 4^2}{3} = \frac{16x}{3} \quad \dots\dots\dots \text{(i)}$$

Now on doubling the volume concentrations will become half of initial so



$$Q_C = \frac{x \cdot 4 \times 2}{2 \times 3} = \frac{4x}{3} < K_C$$

Conc. at new equilibrium (1.5 - a) 2 + 2a

$$\left(\frac{x}{2} + a \right) \text{ Hence forward shift.}$$

Now given that (2 + 2a) = 3

$$\text{so } a = 0.5$$

$$\text{so } [\text{A}] = 1\text{M} \quad [\text{B}] = 3 \quad [\text{C}] = \frac{1}{2}(x+1)$$

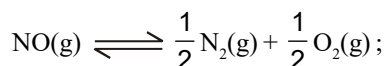
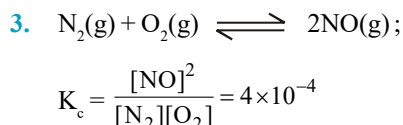
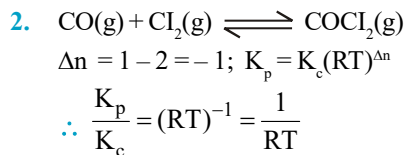
$$\text{so } K_C = \frac{(1+x) \times 9}{2 \times 1} = \frac{16x}{3}$$

$$\text{so } 27x + 27 = 32x$$

$$\text{so } x = \frac{27}{5} = 5.4 \text{ and } K_C = \frac{16}{3} \times \frac{27}{5} \times \frac{144}{5} = 28.8. \text{ Ans.}$$

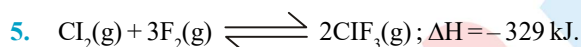
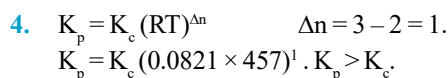
EXERCISE - 5

Part # 1 : AIEEE/JEE-MAIN



$$K_c = \frac{[\text{N}_2]^{1/2}[\text{O}_2]^{1/2}}{[\text{NO}]} = \frac{1}{\sqrt{K_c}} = \frac{1}{\sqrt{4 \times 10^{-4}}} = \frac{1}{2 \times 10^{-2}}$$

$$= \frac{100}{2} = 50$$



Favourable conditions:

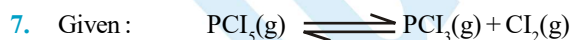
- (i) Decrease in temperature,
- (ii) Addition of reactants,
- (iii) Increase in pressure i.e., decrease in volume.



Initial presens	0	0.5	0
At equi.	0	0.5+x	x

Total pressure = $0.5 + 2x = 0.84$ $\therefore x = 0.17 \text{ atm}$

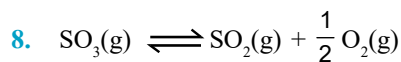
$K_p = P_{\text{NH}_3} \times P_{\text{H}_2\text{S}} = 0.11 \text{ atm}^2$.



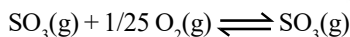
t = 0	1	0	0
t _{eq}	1-x	x	x

Total number of moles = $1 - x + x + x = 1 + x$

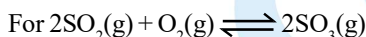
Thus partial pressure of $\text{PCl}_3 = \left(\frac{x}{1+x}\right)P$.



$$\frac{[\text{SO}_2][\text{O}_2]^{1/2}}{[\text{SO}_3]} = K_c = 4.9 \times 10^{-2} \quad \dots\dots\dots \text{(i)}$$



$$\frac{[\text{SO}_3]}{[\text{SO}_2][\text{O}_2]^{1/2}} = K'_c = \frac{1}{4.9 \times 10^{-2}} \quad \dots\dots\dots \text{(ii)}$$



$$\frac{[\text{SO}_3]^2}{[\text{SO}_2]^2[\text{O}_2]} = K_c^2 = \frac{1}{4.9 \times 4.9 \times 10^{-4}} = \frac{10000}{24.01}$$

$$= 416.49$$

9. $c = a + b$



$$K_{P_1} = \frac{\left(\frac{2\alpha}{1+\alpha}P_{T_1}\right)^2}{\left(\frac{1-\alpha}{1+\alpha}P_{T_1}\right)} \quad K_{P_2} = \frac{\left(\frac{\alpha}{1+\alpha}P_{T_2}\right)\left(\frac{\alpha}{1+\alpha}P_{T_2}\right)}{\left(\frac{1-\alpha}{1+\alpha}P_{T_2}\right)}$$

$$\frac{K_{P_1}}{K_{P_2}} = \frac{\left(\frac{2\alpha}{1+\alpha}P_{T_1}\right)^2}{\left(\frac{1-\alpha}{1+\alpha}P_{T_2}\right)} \times \frac{\left(\frac{1-\alpha}{1+\alpha}P_{T_2}\right)}{\left(\frac{\alpha}{1+\alpha}P_{T_2}\right)\left(\frac{\alpha}{1+\alpha}P_{T_2}\right)}$$

$$\frac{1}{9} = \frac{4P_{T_1}}{P_{T_2}}; \quad \frac{P_{T_1}}{P_{T_2}} = \frac{1}{36}$$

11. $PV = nRT$

$V = 1 \text{ dm}^3 = 10^{-3} \text{ m}^3$

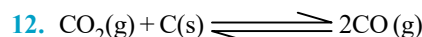
$P = 3170 \text{ Pa}$

$R = 8.314 \text{ J K}^{-1} \text{ mol}^{-1}$

$T = 300 \text{ K}$

$3170 \times 10^{-3} = n \times 8.314 \times 300$

$$n = \frac{3170 \times 10^{-3}}{8.314 \times 300} = 1.27 \times 10^{-3} \text{ mol.}$$



0.5 atm

$$\begin{aligned} 0.5 - p & \quad 2p \\ \text{Total pressure} &= 0.5 - p + 2p = 0.8 \\ p &= 0.3 \end{aligned}$$

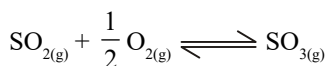
$$K_p = \frac{P_{\text{CO}}^2}{P_{\text{CO}_2}} = \frac{(2p)^2}{(0.5 - p)} = \frac{(0.6)^2}{(0.5 - 0.3)}$$

$$K_p = 1.8$$

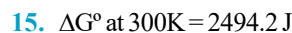


$$\text{NO} \longrightarrow \frac{1}{2}\text{N}_2 + \frac{1}{2}\text{O}_2 \quad K' = \frac{1}{\sqrt{K}} = \frac{1}{\sqrt{4 \times 10^{-4}}} = 50$$

14. For reaction :



$$\Delta N_g = -\frac{1}{2} = x$$



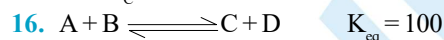
$$\Delta G^\circ = -RT \ln K$$

$$-2494.2 = -8.314 \times 300 \ln K$$

$$K = 10$$

$$Q = \frac{[B][C]}{[A]^2} = \frac{2 \times \frac{1}{2}}{\left(\frac{1}{2}\right)^2} = 4$$

$Q > K_c \Rightarrow$ reverse direction.



$$\begin{array}{cccc} 1 & 1 & 1 & 1 \end{array}$$

$$Q_c = 1 < K_{eq}$$

\therefore forward shift

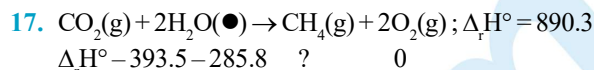
$$t_{eq} \quad n-x \quad (1-x) \quad (1+x) \quad (1+x)$$

$$\frac{(1+x)(1+x)}{(1-x)(1-x)} = 100 \Rightarrow \frac{1+x}{1-x} = 10$$

$$1+x = 10-10x$$

$$x = \frac{9}{11}$$

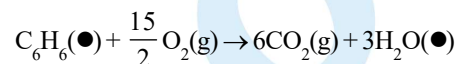
$$\therefore [D] = 1+x = 1 + \frac{9}{11} = 1.818 \text{ Ans.}$$



$$\Delta_r H^\circ = \sum (\Delta_f H^\circ)_{\text{products}} - \sum (\Delta_f H^\circ)_{\text{reactants}}$$

$$890.3 = [1 \times (\Delta_f H^\circ)_{\text{CH}_4} + 2 \times 0] - [1 \times (393.5) + 2(285.8)]$$

$$(\Delta_f H^\circ)_{\text{CH}_4} = 890.3 - 965.1 = -74.8 \text{ kJ/mol}$$



Part # II : IIT-JEE ADVANCED

1. When nitrogen is added at equilibrium condition, the equilibrium will shift according to Le-chatelier principle at equilibrium $\Delta G = 0$ and catalyst changes the rate of forward and backward reactions by equal extent. K_p of reaction is a function of temperature only.

2. $\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ = -54.07 \times 1000 - 298 \times 10$
 $= -54070 - 2980 = -57050$

$$\Delta G^\circ = -2.303 RT \log_{10} K$$

$$-57050 = -2.303 \times 298 \times 8.314 \log_{10} K$$

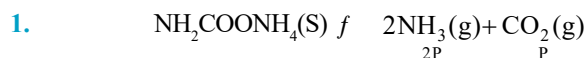
$$= -5705 \log_{10} K$$

$$\log_{10} K = 10$$

3. At equilibrium ΔG (Gibbs energy) = 0 but ΔG° (standard Gibbs energy) $\neq 0$

As ΔG (Gibbs energy) is more negative reaction will be more spontaneous.

MOCK TEST

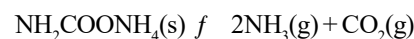


Initial

$$K_p = (P_{\text{NH}_3})^2 (P_{\text{CO}_2})$$

$$K_p = (2P)^2 (P) \dots (i)$$

$$P_T(\text{initial}) = 3P$$



Final

3P

P'

$$K_p = (3P)^2 (P') \dots (ii)$$

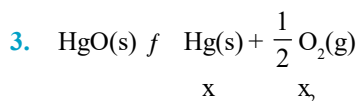
From eq. (i) and (ii)

$$(2P)^2 (P) = (3P)^2 (P')$$

$$P' = \frac{4P}{9}$$

$$\frac{P_T(\text{New})}{P_T(\text{Old})} = \frac{3P + P'}{3P} = \frac{3P + \frac{4P}{9}}{3P} = \frac{31}{27}$$

2. Formation of ammonia is an exothermic process therefore it is favourable at lower temperature. But at lower temperature rate of the reaction becomes slow.



$$K_p = P_{\text{Hg(g)}} \times (P_{\text{O}_2})^{\frac{1}{2}}$$

$$\text{Total moles at equilibrium} = \frac{3x}{2}$$

$$P_{\text{Hg}} = \frac{x}{3x/2} = \frac{2}{3}P$$

$$P_{\text{O}_2} = \frac{x/2}{3x/2} P = \frac{1}{3}P$$

$$K_p = \frac{2}{3}P \left(\frac{1}{3}P \right)^{1/2} = \frac{2}{3^{3/2}} P^{3/2}$$

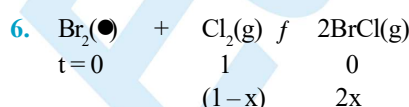
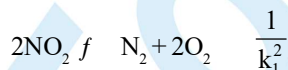


$$\text{Initial conc.} \quad \frac{10^{-3}}{56} \quad b \quad 0$$

$$\text{Final conc.} \quad \frac{10^{-3}}{56} - 6 \times 10^{-6} \quad b - 6 \times 10^{-6} \quad 6 \times 10^{-6}$$

$$K = \frac{10^3}{7.142}$$

$$\text{on solving } b = 0.0036 \text{ M}$$



$$k_p = \frac{(P_{\text{BrCl}})^2}{P_{\text{Cl}_2}} = 1 \text{ so, } P_{\text{Cl}_2} = (P_{\text{BrCl}})^2 = 0.01 \text{ atm}$$

$$\text{then at equilibrium, } \frac{n_{\text{BrCl}}}{n_{\text{Cl}_2}} = \frac{0.1}{0.01} = 10 = \frac{2x}{1-x}$$

$$\text{So, } 10 - 10x = 2x \quad \text{or} \quad x = \frac{10}{12} = \frac{5}{6} \text{ moles}$$

Moles of Br₂(●) required for maintaining vapour pressure of 0.1 atm

$$= 2 \times \frac{5}{6} \text{ moles} = \frac{10}{6} \text{ moles} = \text{moles of BrCl(g).}$$

Moles required for taking part in reaction = moles of Cl₂

$$\text{used up} = \frac{5}{6} \text{ moles.}$$



$$t = 0 \quad 5 \quad 0 \quad 0$$

$$t = t_{\text{eq}} \quad 5 - 5 \times 0.2 \quad 5 \times 0.2 \quad 5 \times 0.2$$

$$4 \text{ mole} \quad 1 \text{ mole} \quad 1 \text{ mole}$$

$$\text{Total moles at equilibrium} = 4 + 1 + 1 + 1 (N_2) = 7 \text{ moles}$$

$$k_p = \frac{\left(\frac{1}{7} \times 1 \text{ atm} \right) \left(\frac{1}{7} \times 1 \text{ atm} \right)}{\left(\frac{4}{7} \times 1 \text{ atm} \right)} = \frac{1}{28} \text{ atm.}$$

10. Given $K_c < 2$ therefore in case of B and C $K_c = \frac{2 \times 4}{6} = \frac{4}{3}$

and concentrated of PCl₃ and Cl₂ together will decrease or increase as reaction can go in the forward or backward direction.



$$t = 0 \quad a \quad 0$$

$$t \quad a(1-\alpha) \quad 2a\alpha$$

$$\text{vapour density} = \frac{46}{1+\alpha} = 30.67$$

$$\text{so } 1 + \alpha = 1.5 = 0.5 = 50 \%$$

$$\text{Total pressure} = \frac{1.5 \times 1.5 \times 0.082 \times 300}{8.2} = 6.75 \text{ atm}$$

$$\text{so } k_p = \frac{4\alpha^2}{1-\alpha^2} P = 9 \text{ atm}$$

$$\text{and for density of mixture} = \frac{138}{8.2} \text{ gm/L} = 16.83 \text{ gm/L.}$$

13. (A) As reaction is endothermic therefore it will go in the



forward direction hence moles of CaO will increase.

(C) With the increase or decrease of volume particle pressure of the gases will remain same.

(D) Due to the addition of inert gas at constant pressure reaction will proceed in the direct in which more number of gaseous moles are formed.

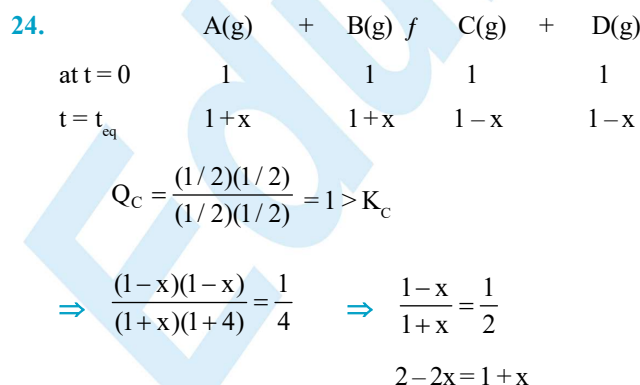
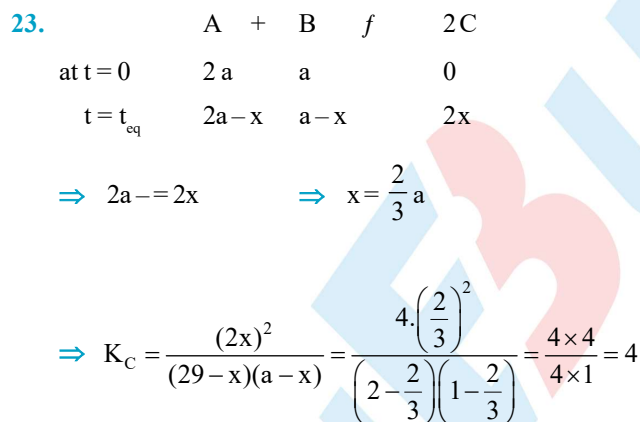
15. As concentration of reaction (gaseous) are increased at equilibrium reaction will go in the forward direction.

Also above reaction is endothermic therefore increase in temperature will favour it.

19. Solubility of gas is favourable at high pressure and this process is exothermic hence solubility will be more at low temperature.

20. Since density of gold decreases after melting therefore it is favourable at low pressure and high temperature.

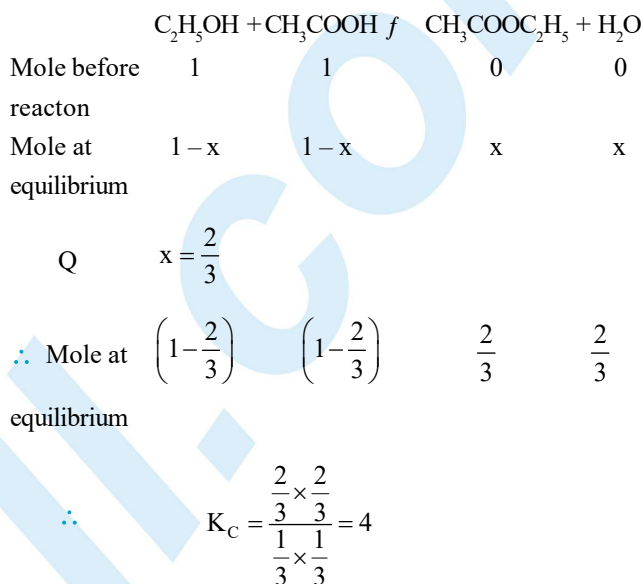
22. Since the slope of the straight line graph between $\log K$ and $\frac{1}{T}$ is positive, $\Delta H_{\text{reaction}}$ would be negative, i.e., the forward reaction would be exothermic.



$$\Rightarrow x = \frac{1}{3}$$

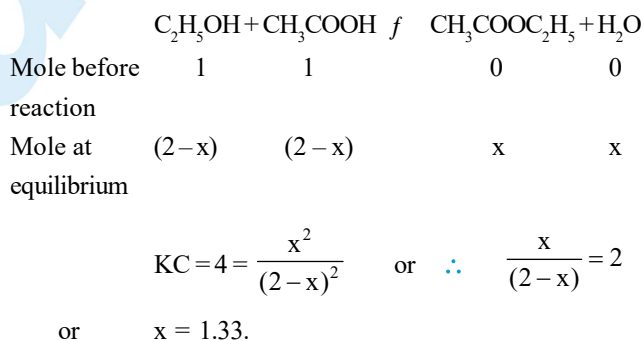
$$\therefore [C] = \frac{1-x}{2} = \frac{1}{3}M$$

25. Case - I



Note: Volume terms are eliminated

Case - II



26. (A - p, t); (B - q, r); (C - q, s)

- (A) $\Delta_{\text{ng}} = 0$ so independent of pressure
Exothermic so high temperature
(B) $\Delta_{\text{ng}} = (-)$ ve High pressure
Exothermic so Low Temperature
(C) $\Delta_{\text{ng}} = (+)$ ve so low pressure
Exothermic so Low Temperature

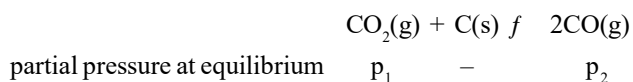
28. (A) As $\Delta n > 0$ therefore if $P \uparrow$, reaction will go in the backward direction.

(B) As $\Delta n < 0$ therefore if $V \uparrow, P \downarrow$ reaction will go in the direction in which more number of gaseous moles are formed i.e. backward direction.

(C) As $\Delta n = 0$ hence no effect.

(D) If concentrated of product is decreased reaction will go in the forward direction.

30. 195488.



$$K_p = \frac{P_2^2}{P_1} = 10 \quad \text{or} \quad P_1 = 0.1 P_2^2 \quad \dots(1)$$

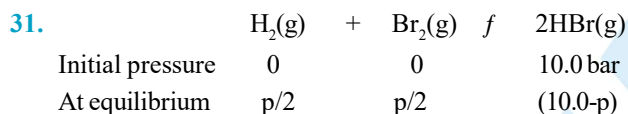
but $p_1 + p_2 = 5.6 \text{ atm}$

solving $p_1 = 1.6 \text{ atm}$ and $p_2 = 4 \text{ atm}$

using $p = \text{CRT}$

$$C_1 (\text{for } \text{CO}_2) = \frac{1.6}{0.082 \times 1000} = 0.0195 \text{ M}$$

$$C_2 (\text{for } \text{CO}) = \frac{4.0}{0.082 \times 1000} = 0.0488 \text{ M.}$$



$$K_p = \frac{p_{\text{HBr}}^2}{P_{\text{H}_2} \times P_{\text{Br}_2}}$$

$$1.6 \times 10^5 = \frac{(10-p)^2}{(p/2)(p/2)}$$

Taking square root of both sides

$$4 \times 10^2 = \frac{10-p}{p/2}$$

$$200 p = 10 - p$$

$$p = \frac{10}{201} \text{ bar}$$

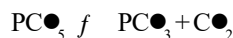
$$P_{\text{H}_2} = p/2 = \frac{1}{2} \left(\frac{10}{201} \right) \text{ bar} = 2.5 \times 10^{-2} \text{ bar}$$

$$P_{\text{Br}_2} = p/2 = 2.5 \times 10^{-2} \text{ bar}$$

$$P_{\text{HBr}} = 10 - p \approx 10 \text{ bar}$$



Let y moles of Cl_2 are introduced then at new equilibrium



$$\therefore \begin{matrix} 2+x & 2-x & 2+y-x \end{matrix} ; \quad \text{Total moles} = 12$$

$$\text{Total moles of } \text{PCl}_5 + \text{PCl}_3 = 4 \text{ and moles of } \text{Cl}_2 = 8$$

$$\therefore P_{\text{PCl}_5} = \frac{(2+x)^3}{12} = \frac{2+x}{4}$$

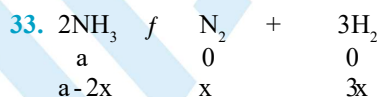
$$P_{\text{PCl}_3} = \frac{(2-x)^3}{12} = \frac{2-x}{4}$$

$$P_{\text{Cl}_2} = \frac{8 \times 3}{12} = 2$$

$$\therefore K_p = 1 = \frac{\left(\frac{2+x}{4} \right) \left(\frac{2}{1} \right)}{\left(\frac{2+x}{4} \right)}$$

$$\therefore x = \frac{2}{3} \text{ and hence from equation (1) } y = \frac{20}{3} = 6.67 \text{ moles}$$

Ans. is 667 – 666



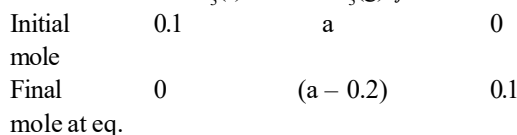
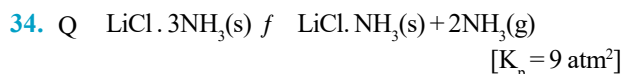
$$\frac{P_1}{T_1} = \frac{P_2}{T_2} \Rightarrow P_2 = 20 \text{ atm.}$$

$$\text{Now } \frac{a+2x}{a} = \frac{30}{20}$$

$$2a + 4x = 3a$$

$$\Rightarrow x = \frac{1}{4} a$$

$$\therefore \% \text{ of } \text{NH}_3 \text{ decomposed} = \frac{2x}{a} \times 100 = 50\%$$



$$\left[K_p = \frac{1}{9} (\text{atm})^{-2} \right]$$

Let initial mole of NH_3 should be a to bring in completed of reaction.

$$\text{At eq. } K_p = \frac{1}{(P'_{\text{NH}_3})^2}$$

$$\text{or } \frac{1}{9} = \frac{1}{(P'_{\text{NH}_3})^2}$$

$$\therefore P'_{\text{NH}_3} = 3 \text{ atm}$$

$$\text{Q } PV = nRT$$

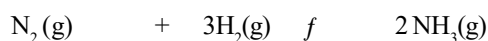
$$3 \times 5 = n \times 0.0821 \times 313$$

$$\therefore n = 0.5837$$

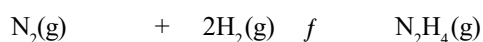
$$\text{i.e., } (a - 0.2) = 0.5837$$

$$\therefore \text{Initial mole of NH}_3 = a = 0.5837 + 0.2 = 0.7837 \text{ mole.}$$

35. Let the initial partial pressures of N_2 and H_2 be $9P$ and $13P$ respectively



$$9P - y - x \qquad 13P - 3x - 2y \qquad 2x$$



$$9P - y - x \qquad 13P - 3x - 2y \qquad y$$

$$\text{Total pressure} = P_{\text{N}_2} + P_{\text{H}_2} + P_{\text{NH}_3} + P_{\text{N}_2\text{H}_4} = 3.5 \text{ atm} \quad \dots(1)$$

$$= (9P - x - y) + (13P - 3x - 2y) + 2x + y = 3.5 \text{ atm} \quad \dots(1)$$

$$P_{\text{NH}_3} = 2x = 0.5 \text{ atm} \quad \dots(2)$$

$$P_{\text{H}_2} = (13P - 3x - 2y) = 1 \text{ atm} \quad \dots(3)$$

$$\text{from (1)} \Rightarrow (9P - x - y) + 1 \text{ atm} + 0.5 + y = 3.5$$

$$\Rightarrow (9P - x) = 2 \text{ atm}$$

$$\text{so } 9P = 2.25$$

$$P = 0.25 \text{ atm}$$

$$\text{from (3) equation } 2y = 1.5$$

$$y = 0.75 \text{ atm}$$

$$\text{so } P_{\text{N}_2} = 9P - x - y = 1.25 \text{ atm}$$

$$P_{\text{H}_2} = 1 \text{ atm}$$

$$P_{\text{NH}_3} = 0.5 \text{ atm}$$

$$P_{\text{N}_2\text{H}_4} = 0.75 \text{ atm}$$

$$\text{So, } K_{p_1} = \frac{P_{\text{NH}_3}^2}{P_{\text{H}_2}^3 \cdot P_{\text{N}_2}} = \frac{0.5 \times 0.5}{1 \times 1 \times 1 \times 1.25} = 0.2 \text{ atm}^{-2}$$

$$K_{p_2} = \frac{P_{\text{N}_2\text{H}_4}}{P_{\text{N}_2} \cdot P_{\text{H}_2}^2} = \frac{0.75}{1 \times 1 \times 1.25} = 0.6 \text{ atm}^{-2}$$