

### impulse turbines -Pelton wheels



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## **Construction and Component**





## Installation



# **Velocity Triangle**

**Euler Equation:** 

 $W/m = U_1 C_{x1} - U_2 C_{x2}$ 

$$W/m = U\{(U + W_1) + [W_2 \cos(180^\circ - \alpha) - U]\}$$

Assume no loss of relative velocity,  $W_1 = W_2$ 

$$W/m = U(W_1 - W_1 \cos \alpha)$$

$$E = U(C_1 - U)(1 - \cos \alpha)/g$$

For maximum  $E \rightarrow dE/dU = 0$  $C_1 = 2U$   $U = C_1/2$ 

$$E_{\max} = C_1^2 (1 - \cos \alpha)/4g$$



# **Velocity Triangle**

In practice :

Surface friction of the bucket  $\rightarrow W_2 \neq W_1$ 

$$E = U(C_1 - U)(1 - k\cos\alpha)/g$$

k is the relative velocity ratio  $W_2/W_1$ 



# **Losses and Efficiency**

Pipeline transmission efficiency  $\rightarrow$  pipeline losses,  $h_f$ 

	$\eta_{\scriptscriptstyle trans} =$	energy at end of pipeline	$- \frac{\left(H_1 - h_f\right)}{\left(H_1 - h_f\right)}$	_ <u>_</u>
		energy available at reservoir	$-H_1$	$\overline{H_1}$

Nozzle efficiency  $\rightarrow$  nozzle losses,  $h_{in}$ 

$$\eta_N = \frac{\text{energy at nozzle outlet}}{\text{energy at nozzle inlet}} = \frac{\left(H_1 - h_f - h_{in}\right)}{\left(H_1 - h_f\right)} = \frac{\left(H - h_{in}\right)}{H} = \frac{H'}{H}$$

Energy available in jet at nozzle outlet :  $|H' = C_1^2/2g|$ 

Nozzle velocity coefficient

 $C_{v} = \frac{\text{actual jet velocity at nozzle outlet}}{\text{theoretical jet velocity at nozzle inlet}} = \frac{C_{1}}{\sqrt{2gH}}$ 

 $high \eta_N = C_v^2$ 

#### Hydraulic efficiency

$$\eta_{H} = \frac{\text{energy transferred}}{\text{energy available in jet at nozzle outlet}} = \frac{E}{H'} = \frac{E}{\left(C_{1}^{2}/2g\right)}$$

## **Losses and Efficiency**

**Overall Efficiency** 

$$\eta_o = \frac{\text{Power developed by the turbine}}{\text{Power available at nozzle inlet}} = \frac{P}{\rho g Q H}$$

### Turbine discharge, Q

$$Q = (\text{nozzlearea})(\text{actual jet velocity at nozzle outlet})$$
$$= AC_1 = (\pi d^2/4)C_1$$

d = nozzle diameter

## Example

A Pelton turbine develops 2000 kW under a head of 100 m and with an overall efficiency of 85%. The coefficient of velocity for the nozzle is 0.98. Determine:

(a) The theoretical velocity of the jet ?

(b) The actual velocity of the jet ?

(c) The flow rate ?

(d) The diameter of the nozzle

#### Solution:

Given: P = 2000 kW; H = 100 m;  $\eta_o = 0.85$ ;  $C_v = 0.98$ Let : d = diameter of the nozzle; Q = discharge flow rate of the turbine

(a) The theoretical velocity of the jet

$$C_{theo} = \sqrt{2gH} = \sqrt{2(9.81)(100)} = 44.3 \text{ m/s}$$

(b) The actual velocity of the jet

$$C_{v} = \frac{C_{1}}{\sqrt{2gH}}$$
  
$$\Rightarrow C_{1} = C_{v}\sqrt{2gH} = C_{v}C_{theo} = (0.98)(44.3) = 43.4 m/s$$

### Example

#### (c) The flow rate

$$\eta_o = \frac{P}{\rho g Q H}$$
  

$$\Rightarrow Q = \frac{P}{\rho g H \eta_o} = \frac{2000.10^3}{(10^3)(9.81)(100)(0.85)} = 2.4 \ m^3 / s$$

#### (d) The diameter of the nozzle

$$Q = AC_1 = (\pi d^2/4)C_1$$
  

$$\Rightarrow d = \sqrt{\frac{4Q}{\pi C_1}} = \sqrt{\frac{4(2.4)}{\pi (43.4)}} = 0.265 m$$

# **Design of Pelton Wheels**

Pelton wheel is designed with the following input:

- 1. Head of water
- 2. Power to be developed
- 3. Speed of the runner

**Pelton wheel is designed to find out the following data:** 

- 1. Diameter of the wheel (D)
- 2. Diameter of the jet (d)
- 3. Size (i.e. width and depth) of the buckets
- 4. Number of buckets (z)

**Pelton wheel is usually designed with the following assumption:** 

- 1. Overall efficiency,  $\eta_o$  between 80% and 87%
- 2. Coefficient of velocity,  $C_v$  as 0.98 to 0.99
- 3. Ratio of peripheral velocity to the jet velocity,  $U/C_1$  as 0.43 to 0.48

# **Design of Pelton Wheels**

#### Size of the buckets



#### Number of the buckets (z)

**Theoretical :** 

$$z = 360^{\circ}/\alpha$$

where:

$$\cos \alpha = \frac{R + 0.5d}{R + 0.6d}$$
$$R = D/2$$

**Empirical**:

$$z = 15 + \frac{D}{2d}$$

## **Characteristics Curves**



## Load Changes

In practice :

*U* must remain constant when the load changes  $\rightarrow$  to maintain maximum efficiency *U*/*C*<sub>1</sub> must stay the same  $\rightarrow$  change the input of water power  $\rightarrow$  change in *Q*  $\rightarrow$  change in nozzle area *A* 



Load Control : spear valve and deflector plate

## **Load Changes**

